

# Rear Interface Engineering in Solution-Processed Submicron Cu(In,Ga)(S,Se)<sub>2</sub> Solar Cells on Transparent Sn:In<sub>2</sub>O<sub>3</sub> Back Contact

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The parasitic absorption in Cu(In,Ga)(S,Se)<sub>2</sub> (CIGSSe) solar cells emerging from the Mo back contact can be significantly reduced by replacing it with tin-doped indium oxide (ITO). Commonly, an undesirable GaO<sub>x</sub> layer forms at the CIGSSe/ITO interface during the high-temperature fabrication process, which has a detrimental effect on photo-carrier extraction. Here, a Cu-In-TU-DMF (TU: thiourea, DMF: N, N-Dimethylformamide) intermediate layer for modification of the CIGSSe/ITO interface, which improves the efficiency of submicron CIGSSe solar cells significantly, is reported about. The reference submicron CIGSSe solar cells exhibit inferior performance (2.4% efficiency) and a large open circuit voltage deficit ( $V_{oc,def} = 815.9$  mV) due to a high barrier at the CIGSSe/ITO interface. At the modified rear interface, the recombination is reduced and hence carrier transport and collection are obviously improved. The efficiency of submicron CIGSSe solar cells on ITO with rear interface modification achieves 7.9% with an open circuit voltage of 565.8 mV, a short circuit current density of 23.4 mA cm<sup>-2</sup>, and a fill factor of 59.5%, as well as a  $V_{oc,def}$  of 589.2 mV.

due to complex fabrication conditions.<sup>[2]</sup> In contrast, solution-processed CIGSSe thin film fabrication presents the potential for cost-effectiveness and high throughput.<sup>[3]</sup> The molecular precursor solution approach has many advantages, such as simple solution preparation, high material utilization rate, adaptability to roll-to-roll processing, precise control of element composition, and large-area homogeneity.<sup>[2a,3e,f,4]</sup> However, the optimal performance of solution-processed CIGSSe solar cells is achieved from a hydrazine-based precursor solution, which prohibits its industrial production for health, environment, and safety concerns.<sup>[3c]</sup> Jiang et al. have proven that efficiencies of 14.5% for CuIn(S,Se)<sub>2</sub> (CISSe) and 15.2% for Cu(In,Ga)(S,Se)<sub>2</sub> (CIGSSe) solar cells can be obtained from a metal-chloride-TU-DMF (TU: thiourea, DMF: N, N-Dimethylformamide) precursor

solution, which offers an alternative path to replace the highly toxic hydrazine precursor process.<sup>[4b]</sup> Furthermore, a reduction of material consumption along with a shortening of the deposition duration can be achieved by thinning the absorber thickness to submicron (absorber thickness < 1 μm). In addition, a submicron CIGSSe absorber can reduce the pathway for electron/hole extraction and improve the homogeneity of the absorber and therefore is promising for cost-effective and efficient solar cells.<sup>[5]</sup>

Typically, molybdenum (Mo) is used as a back contact material for various chalcogenide thin film solar cells due to the formation of the favorable quasi-Ohmic contact at the absorber/Mo interface. However, the Mo back contact has strong parasitic absorption, leading to an increase in optical losses for submicron cells.<sup>[6]</sup> Compared to the opaque Mo back contact, the fabrication of CIGSSe absorbers on transparent conductive oxide (TCO) back contacts can reduce the optical losses of the solar cells and open up further application areas.<sup>[2b,7]</sup> Various TCOs, such as tin-doped indium oxide (ITO), fluorine-doped tin oxide (FTO), and aluminum-doped zinc oxide (AZO), have been used as back contact of CIGSSe solar cells.<sup>[3a,8]</sup> However, the highly resistive GaO<sub>x</sub> layer forming at the CIGSSe/TCO rear interface during the high-temperature CIGSSe growth (temperatures above 520 °C) leads to blocking the hole extraction from the CIGSSe absorber.<sup>[3a,8c]</sup>


## 1. Introduction

The champion efficiency of copper indium gallium disulfoselenide [Cu(In,Ga)(S,Se)<sub>2</sub>: CIGSSe] thin film solar cells has achieved 23.6%, which makes them a promising alternative to silicon solar cells.<sup>[1]</sup> The best-performing CIGSSe solar cells are deposited by vacuum methods, which are expensive techniques

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**Figure 1.** The recipe of CIGSSe absorbers with or without interface treatment.

Therefore, the rear interface composition plays a crucial role in obtaining high-efficient CIGSSe solar cells on TCO.

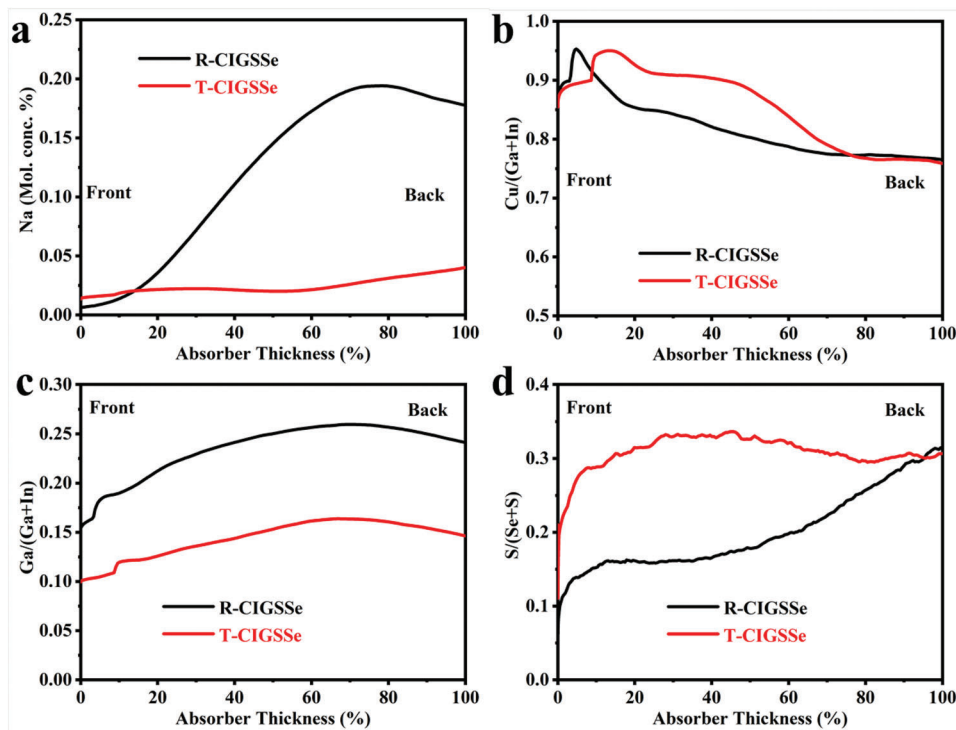
So far, the maximum efficiency achieved for solution-processed CIGSSe on TCO back contacts is only 6%.<sup>[3a]</sup> High-quality CIGSSe solar cells on TCO can be fabricated at low substrate temperature by a co-evaporation process.<sup>[6b,d]</sup> However, when the solution-processed precursor films are selenized at low temperatures, the rear side of the absorber consists of an undesirable fine-grained layer, which can be related to high recombination.<sup>[8a]</sup> Therefore, there are still enormous challenges in fabricating high-quality CIGSSe on TCO back contacts by solution processing. Inserting a thin Mo layer between the CIGSSe and TCO back contact is a potential strategy to overcome this challenge because it allows CIGSSe absorber growth at high temperatures without the formation of  $\text{GaO}_x$ .<sup>[2d,8c,9]</sup> However, the parasitic optical absorption of Mo is a challenge in improving the usage of unabsorbed light supposed to be, e.g., reflected back into the absorber by a reflective mirror from the back side of the glass.<sup>[2b,c,e,6c]</sup> In our previous research, an 8% efficient CISSe (no Ga) solar cell with a submicron absorber has been successfully fabricated on ITO back contact by selenizing the solution-processed metal-chloride-DMF precursor film at 520 °C.<sup>[10]</sup> However, open-circuit voltage ( $V_{oc}$ ) and fill factor ( $FF$ ) are still low, which limits further efficiency improvement. Therefore, CIGSSe solar cells including gallium are favorable due to the expected higher  $V_{oc}$  and efficiency compared to CISSe owing to the widened bandgap with increasing Ga content.<sup>[4b]</sup> Given the achieved good performance of CISSe on ITO, introducing a thin electrically beneficial CISSe layer at the CIGSSe/ITO interface is a potential strategy for achieving high-efficiency CIGSSe solar cells fabricated via the solution process.

In this work, we report on cost-efficient CIGSSe solar cells deposited from metal-chloride-DMF solution on ITO back contact. A thin Cu-In-TU-DMF layer is pre-deposited on the ITO back contact for interface modification before the Cu-In-Ga-TU-DMF precursor solution. This modification layer is applied to reduce the Ga concentration at the rear interface of the CIGSSe absorber. The lower Ga concentration favors obtaining a high-quality CIGSSe absorber and hinders the formation of the  $\text{GaO}_x$  interlayer. The modified interface reduces the back barrier height and significantly improves the photovoltaic (PV) performance. We demonstrate a power conversion efficiency ( $PCE$ ) of 7.9% for this CIGSSe solar cell with a thin Cu-In-TU-DMF interface modification layer.

## 2. Results

**Figure 1** shows the schematic illustration of the structure with/without a Ga-free modification layer (Cu-In-TU-DMF). In brief, the Ga-free layer is firstly spin-coated on ITO back contact.

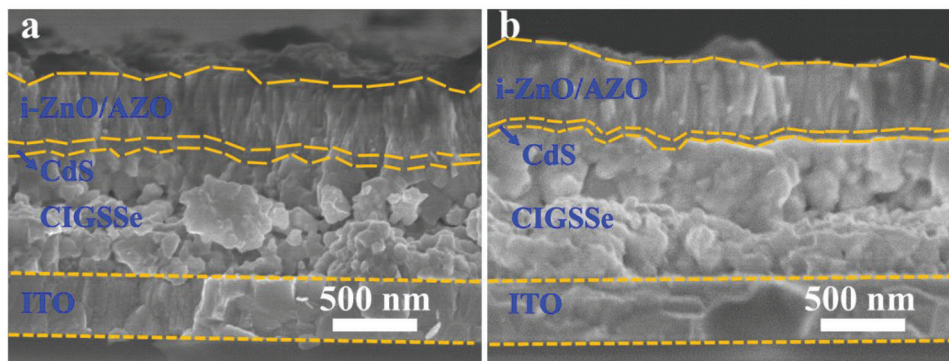
The elemental distributions of the absorbers are measured by GD-OES and are presented in **Figure 2** and Figure S1 (Supporting Information). Both reference CIGSSe (R-CIGSSe) and interface modification treatment CIGSSe (T-CIGSSe) show lower Na concentrations near the front surface than in the absorber bulk (Figure 2a). The R-CIGSSe absorber presents a significantly higher Na concentration in the bulk of the absorber (from 15% depth toward the rear surface) than the T-CIGSSe absorber. However, a reverse trend is observed near the front surface (0–15% depth). The T-CIGSSe absorber displays a mostly uniform and low concentration of Na, which can be attributed to a small amount of Na diffusing into the T-CIGSSe absorber from the SLG substrate. In the solution process, high-quality and dense chalcopyrite absorbers grow from the liquid-phase  $\text{Cu}_{2-x}\text{Se}$  compound.<sup>[4b]</sup> Compared to the lattice constant of  $\text{CuGaSe}_2$  (0.560 nm),  $\text{CuInSe}_2$  (0.578 nm) and  $\text{Cu}_{2-x}\text{Se}$  (0.579 nm) have highly similar lattice constants, resulting in the formation of a dense layer on the bottom of the T-CIGSSe absorber.<sup>[11]</sup> From this, it is concluded that the T-CIGSSe absorber receives a lower Na concentration than the R-CIGSSe absorber. A high Na content will promote  $\text{GaO}_x$  formation during the absorber growth at a high temperature.<sup>[12]</sup> Therefore, this thin In-rich interface modification layer favors the formation of a dense benign electrical rear interface, which can reduce the diffusion of Na, resulting in hindering the  $\text{GaO}_x$  formation. As can be seen in Figure 2b, the Cu/(Ga+In) (CGI) ratio in R-CIGSSe and T-CIGSSe absorbers increases toward the front surface, yet drops in its direct vicinity. The T-CIGSSe absorber shows a wider Cu-depletion at the front surface compared to the R-CIGSSe absorber. Na can occupy Cu vacancies ( $\text{Na}_{Cu}$ ) of the CIGSSe absorber, leading to a low Cu concentration in the bulk of the R-CIGSSe absorber (15–70% absorber depth) with a relatively high Na concentration.<sup>[4b,13]</sup> Both of these two CIGSSe absorbers exhibit a similar tendency of Ga/(In+Ga) ratio (GGI) (Figure 2c), which can be attributed to the inter-diffusion of In and Ga. Ga diffuses toward the rear side and In migrates toward the front side of the absorber.<sup>[2a,6a,8c,11]</sup> The maximum GGI occurs at a depth of  $\approx 70\%$ . Simultaneously, an overall larger GGI exists in the R-CIGSSe absorber than in the T-CIGSSe absorber due to the lack of a Ga-free modification layer in R-CIGSSe (Figure 1). A pronounced



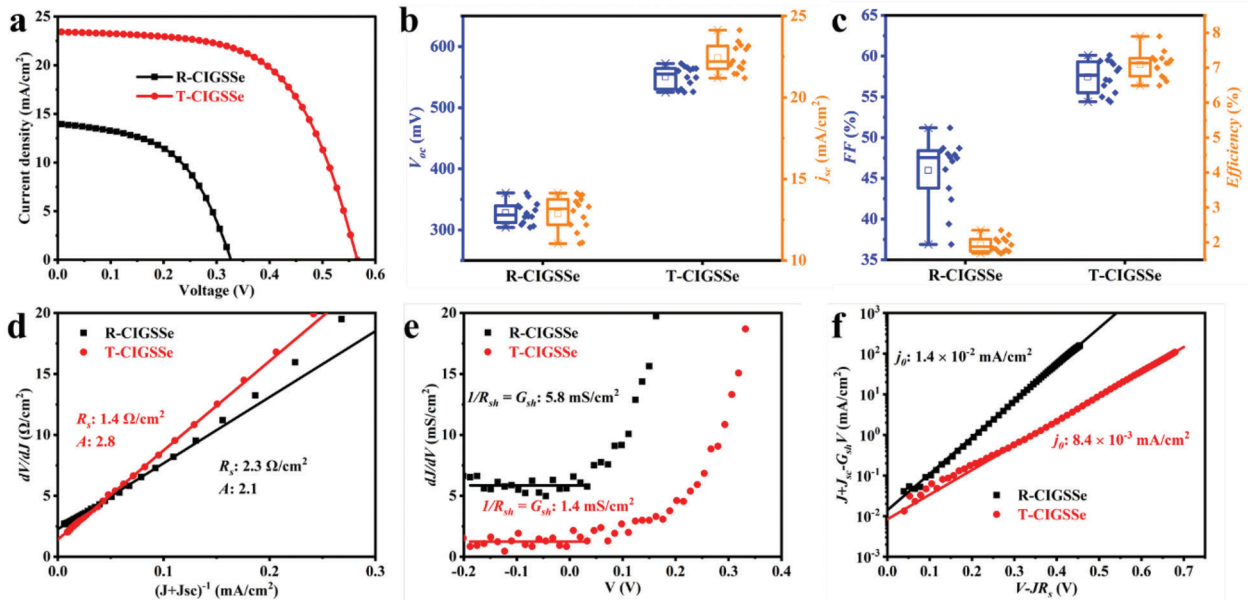
**Figure 2.** a) Na concentration profiles, b) Cu/(Ga+In), c) Ga/(Ga+In), and d) S/(Se+S) ratios of absorbers measured by GDOES. The x-axis is normalized to 100% absorber thickness.

increase in the S/(Se+S) ratio toward the rear interface is observed in the R-CIGSSe absorber in contrast to a high and homogeneous distribution for T-CIGSSe (Figure 2d). It is reported that  $\text{In}_2\text{S}_3$  shows a lower standard molar formation enthalpy ( $-427.0 \text{ kJ mol}^{-1}$ ) at 298.15 K than  $\text{In}_2\text{Se}_3$  ( $-78 \text{ kJ mol}^{-1}$ ), indicating that  $\text{In}_2\text{S}_3$  forms easier than  $\text{In}_2\text{Se}_3$ . T-CIGSSe presents a higher CGI than R-CIGSSe in the 15–70% absorber depth (Figure 2b), which can benefit large grain formation and reduce the grain boundaries.<sup>[14]</sup> However, the volatilization of elemental S is along the grain boundaries. The formation of  $\text{In}_2\text{S}_3$  and reduction of grain boundaries hinder the volatilization of elemental S in the T-CIGSSe (S comes from the thiourea of the precursor solution), leading to the high concentration of S in the T-CIGSSe absorber.

Cross-sectional SEM images of the CIGSSe devices are shown in Figure 3. The thicknesses of the CIGSSe absorbers are 730 nm. The R-CIGSSe absorber can be divided into an  $\approx 300 \text{ nm}$  thick layer with small grains on top and a 400 nm thick layer with a non-uniform size of CIGSSe grains on the bottom (Figure 3a). Larger grains on the bottom can be attributed to the high content of Na (Figure 2a). Unlike the R-CIGSSe absorber, a large-grained top layer of  $\approx 450 \text{ nm}$  is observed in the T-CIGSSe absorber (Figure 3b), which can be explained by a slightly higher Na content near the front surface (0–15% depth of absorber) of the T-CIGSSe. A continuous dense bottom layer is observed in the T-CIGSSe. It has been proven that CIGSe and  $\text{Cu}_{2-x}\text{Se}$  have a similar lattice constant, and the CIGSe absorber is denser than the CGSe absorber.<sup>[10]</sup> When the absorbers have similar Cu



**Figure 3.** Cross-sectional SEM images of the a) R-CIGSSe and b) T-CIGSSe device.



**Figure 4.** a)  $J$ - $V$  curves of the best CIGSse solar cells; b) statistical distributions of open circuit voltage  $V_{oc}$ , short current density  $j_{sc}$ , c) fill factor  $FF$  and efficiency derived from 14 devices for each fabrication method; d)  $dV/dJ$  as a function of  $1/(J + J_{sc})$  with a linear fit to extract  $R_s$  from the y-intercept and  $A$  from slope, e)  $dV/dJ$  versus  $V$  for  $R_{sh}$  extraction, f)  $\ln(J+J_{sc}-G_{sh}V)$  versus  $V-JR_s$  with fit to determine  $j_0$ . (d–f) refer to the best CIGSse solar cells.

content, the In-rich absorber consists of uniform and dense grains rather than the Ga-rich absorber.<sup>[11]</sup> As both absorbers show similar CGI ratios in 75–100% depth (Figure 2b), the dense bottom layer of the T-CIGSse absorber consisting of uniform grains is ascribed to the smaller GGI (Figure 2c).

Figure 4a presents the current density-voltage ( $J$ - $V$ ) curves of the best R-CIGSse and T-CIGSse devices. A power conversion efficiency ( $PCE$ ) of 2.4% is obtained for the R-CIGSse solar cell with  $V_{oc} = 327.1$  mV,  $j_{sc} = 14.0$  mA cm<sup>-2</sup>, and  $FF = 51.2\%$ . When a Cu-In-TU-DMF layer is applied for rear interface modification, the  $PCE$  of the resulting T-CIGSse device is significantly improved to 7.9% with  $V_{oc} = 565.8$  mV,  $j_{sc} = 23.4$  mA cm<sup>-2</sup>, and  $FF = 59.5\%$ . The improvement of  $PCE$  of the T-CIGSse device can be ascribed to the remarkable increase in  $V_{oc}$  and  $j_{sc}$ . The statistical distributions of the photovoltaic parameters for 14 CIGSse sub-cells of each recipe are shown in Figure 4b,c.  $PCE$ ,  $V_{oc}$ ,  $j_{sc}$ , and  $FF$  of the T-CIGSse devices are superior to those of the R-CIGSse devices, implying that the rear interface modification is an effective strategy to obtain high-efficiency CIGSse solar cells on TCO.

The series resistance ( $R_s$ ), the shunt conductance ( $G_{sh}$ ), the shunt resistance ( $R_{sh}$ ), the ideality factor ( $A$ ), and the reverse saturation current density ( $j_0$ ) are calculated from the illuminated  $J$ - $V$  curves by applying the Hegedus method to the equation<sup>[2b,10,15]</sup>:

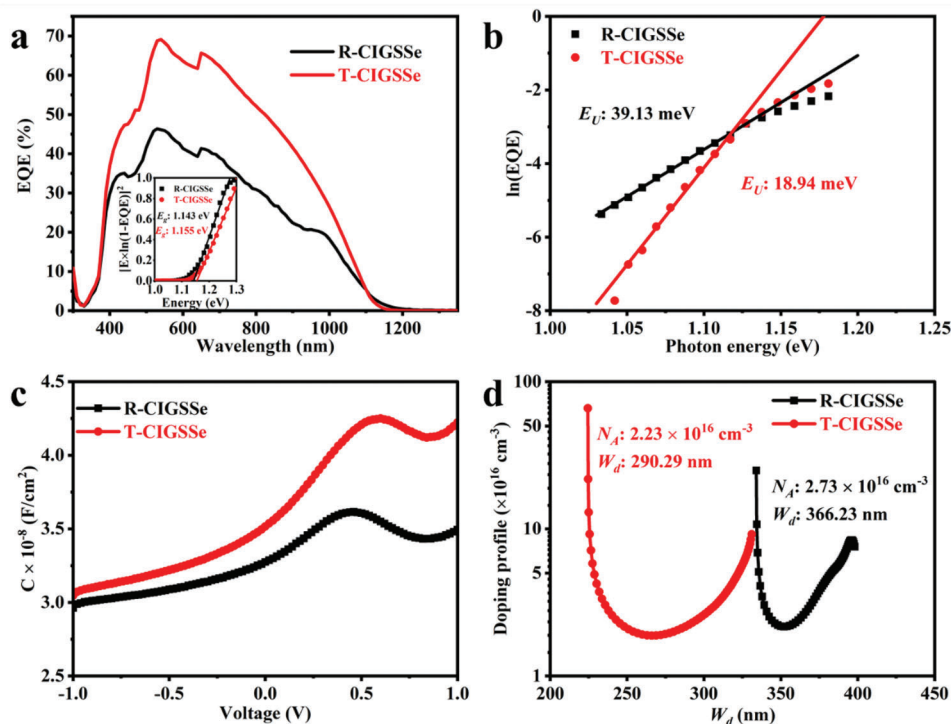
$$j(V) = j_0 \exp \left[ \frac{q}{AkT} (V - jR_s) \right] + G_{sh} V - j_{sc} \quad (1)$$

**Table 1.** Photovoltaic parameters of the best CIGSse device with or without interface modification.

	$PCE$ [%]	$V_{oc}$ [mV]	$j_{sc}$ [mA cm <sup>-2</sup> ]	$FF$ [%]	$R_s$ [ $\Omega$ cm <sup>2</sup> ]	$G_{sh}$ [mS cm <sup>-2</sup> ]	$R_{sh}$ [ $\Omega$ cm <sup>2</sup> ]	$A$	$j_0$ [mA cm <sup>-2</sup> ]
R-CIGSse	2.4	327.1	14.0	51.2	2.3	5.8	178.1	2.1	$1.4 \times 10^{-2}$
T-CIGSse	7.9	565.8	23.4	59.5	1.4	1.4	714.3	2.8	$8.4 \times 10^{-3}$

where  $q$  is the elementary charge and  $k$  the Boltzmann constant. The resulting electrical parameters are presented in Figure 4 and are summarized in Table 1. The best T-CIGSse device exhibits a smaller  $R_s$  and a larger  $R_{sh}$ , indicating that the Cu-In-TU-DMF interface modification can improve the charge transport and reduce the recombination (bulk and interface recombination) (Figure 4d,e).<sup>[2d,8c]</sup> The smaller  $j_0$  in the T-CIGSse device confirms reduced bulk recombination (Figure 4f). Therefore, the T-CIGSse device presents better PV performance. However, the ideality factor is higher with interface modification (Figure 4d and Table 1), which can be explained by the high Na content near the front surface of the T-CIGSse absorber (Figure 2).<sup>[16]</sup> This high Na-content will occupy the Cu vacancies and form Na<sub>Cu</sub> defects, which will hinder the Cd<sup>2+</sup> diffusion and formation of Cd<sub>Cu</sub> donor defects during the CdS chemical bath deposition process. Yet, the PV performance of T-CIGSse solar cells is still superior to one of the R-CIGSse devices, indicating that the front surface is not the main reason for limiting the efficiency of CIGSse solar cells.

EQE measurements of the respectively best R-CIGSse and T-CIGSse devices are depicted in Figure 5a. They show a similar EQE in the short wavelength range (300–390 nm). Yet, the T-CIGSse device exhibits a significantly higher spectral response from 390 to 1100 nm wavelength. The bandgap ( $E_g$ ) values of the two cells are obtained from the plot of  $[E \ln(1-EQE)]^2$  versus  $E$ .<sup>[10]</sup> The  $E_g$  of R-CIGSse is 1.143 eV, while it is 1.155 eV for T-CIGSse (inset in Figure 5a). The slight increase in  $E_g$  by



**Figure 5.** a) External quantum efficiency, inset: bandgap extraction, b)  $\ln(\text{EQE})$  as a function of photon energy at the long-wavelength edge to determine the Urbach energy  $E_U$ , c)  $C$ - $V$  curves, and d) doping profiles for the best R-CIGSSe and T-CIGSSe solar cell.

0.012 eV can be ascribed to the higher S content of the T-CIGSSe absorber (Figure 2d). The Urbach energy ( $E_U$ ) can be extracted from the EQE at the long-wavelength edge and reflects the carrier mobility and lifetime of the solar cells.<sup>[16]</sup> Figure 5b shows the according relation between  $\ln(\text{EQE})$  and photon energy:  $E_U = 39.13$  meV is obtained for the R-CIGSSe solar cell and reduces to 18.94 meV for T-CIGSSe, implying a significantly improved absorber quality.<sup>[16]</sup> The deficit in open circuit voltage,  $V_{oc,def}$ , calculated as the difference of this bandgap value (divided by the elementary charge) and the open circuit voltage from Table 1, is given in Table 2. It reduces from 815.9 to 589.2 mV, i.e., by > 25% relative, with interface modification, and can partially be explained by a smaller  $E_U$  value of the T-CIGSSe device.<sup>[16a]</sup>

Figure 5d shows the acceptor doping density ( $N_A$ ) and the width of the depletion region ( $W_d$ ) of the highest efficient CIGSSe solar cells of each type extracted from the room temperature  $C$ - $V$  profiles (Figure 5c). The R-CIGSSe device exhibits a larger  $N_A$  and a wider  $W_d$  than the T-CIGSSe one (Figure 5d and Table 2), which may originate from the high Na content in the bulk and the low Na content near the front surface of the R-CIGSSe absorber (Figure 2a), leading to increased charge carrier concentration and improved pn-junction formation, respectively. Generally, a wide  $W_d$  can promote the separation of photo-generated electron-hole

pairs and benefit carrier transportation.<sup>[17]</sup> However, the PV performance of the R-CIGSSe device is significantly inferior. Therefore, the limitation of high-efficiency achievement in R-CIGSSe may come from the CIGSSe/ITO interface.

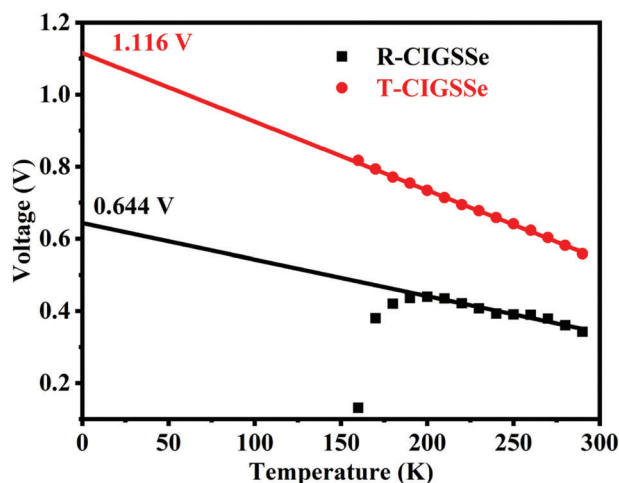
Figure 6 shows the temperature versus voltage plot obtained from temperature-dependent current density-voltage measurements of the CIGSSe solar cells. The activation energy  $E_a$  can be extracted from the  $JV(T)$  profiles by linear extrapolation of  $V_{oc}$  to  $T = 0$  K according to the equation<sup>[2b,6b]</sup>:

$$V_{oc} = \frac{E_a}{q} - \frac{AkT}{q} \ln\left(\frac{j_{00}}{j_{sc}}\right) \quad (2)$$

where  $j_{00}$  denotes the prefactor of saturation current density. Generally, when CIGSSe absorbers are fabricated on Mo back contact,  $E_a$  is close to  $E_g$  owing to a quasi-Ohmic contact assisted by the formation of  $\text{Mo}(\text{S,Se})_2$ . However, there is a non-negligible back barrier ( $\Phi_B$ ) remaining at the CIGSSe/ITO interface. The sheet resistance of the as-sputtered ITO back contact is  $32.02 \Omega \text{ sq}^{-1}$  and it can reduce to  $17.14 \Omega \text{ sq}^{-1}$  after being subjected to pre-annealing at  $500^\circ\text{C}$  for 10 min (Figure S2, Supporting Information). The sheet resistance of the ITO back contact in the completed CIGSSe solar cells further reduces to  $9.15 \Omega \text{ sq}^{-1}$ , which is

**Table 2.** Optoelectronic device properties of the best R-CIGSSe and the best T-CIGSSe solar cells.

	$E_g$ [eV]	$E_U$ [meV]	$N_A$ [ $\text{cm}^{-3}$ ]	$W_d$ [nm]	$E_a$ [eV]	$V_{oc,def}$ [mV]	$\Phi_B$ [eV]
R-CIGSSe	1.143	39.13	$2.73 \times 10^{16}$	366.23	0.644	815.9	0.499
T-CIGSSe	1.155	18.94	$2.23 \times 10^{16}$	290.29	1.116	589.2	0.039



**Figure 6.** Temperature-dependent open-circuit voltage of CIGSs solar cells and linear extrapolations to  $T = 0$  K.

measured by mechanically removing the CIGSs absorber. However, this sheet resistance is still higher than the  $0.3 \Omega \text{ sq}^{-1}$  for Mo after CIGSs removal. Therefore,  $E_g - \Phi_B$  should be considered in Equation (2) rather than  $E_a$ , and the back barrier height can be extracted as  $\Phi_B = E_g - E_a$ .<sup>[2b,6b]</sup>

A small value of  $E_a = 0.644$  eV is observed for the R-CIGSs device, revealing a large gap compared with  $E_g$  and thus pointing to interface recombination (Figure 6 and Table 2).<sup>[6b,18]</sup> There are two interfaces in the CIGSs absorber: the CdS/CIGSs front interface and the CIGSs/ITO rear interface. The R-CIGSs device has a smaller recombination rate at the depletion region than the T-CIGSs device, which is identified by  $J-V$  measurements (small ideality factor). These results reveal that the main limitation for achieving high efficiency of the R-CIGSs device is the serious rear interface recombination and the back barrier  $\Phi_B$  amounting to 499 meV. On the contrary, for the T-CIGSs device,  $E_a$  is significantly improved to 1.116 eV, i.e., only 39 meV (equal to  $\Phi_B$ ), smaller than  $E_g$  (Figure 5b). Thus, the dominant recombination mechanism in the T-CIGSs devices is bulk recombination rather than interface recombination.<sup>[6b]</sup> These results indicate that the dominant recombination path of the CIGSs device can be changed from interface recombination to bulk recombination by utilizing Cu-In-TU-DMF for rear interface modification.

Combining the  $J-V$  and the  $JV(T)$  results, we derive the order of dominant recombination paths of these two CIGSs devices: R-CIGSs interface recombination (dominant recombination) > R-CIGSs bulk recombination > T-CIGSs bulk recombination (dominant recombination) > T-CIGSs interface recombination and conclude that recombination can be significantly suppressed by the interface modification.

### 3. Conclusion

In summary, we have demonstrated that a Cu-In-TU-DMF layer for modifying the CIGSs/ITO interface leads to a significant improvement in the device's performance. The T-CIGSs device hence has a larger shunt resistance and a smaller reverse saturation current density than the R-CIGSs device, confirming that

the bulk recombination can be mitigated by interface modification. The open circuit voltage deficit of the T-CIGSs device is significantly smaller than for R-CIGSs, which can also be explained by the better absorber quality (smaller Urbach energy). The R-CIGSs device has a smaller ideality factor, larger charge carrier density, and depletion width values. Yet, a significantly smaller value of barrier height is observed for the T-CIGSs device, indicating that the rear interface modification is a simple and effective strategy to reduce interface recombination and improve the properties of submicron CIGSs solar cells on TCO back contact. As a result, the champion efficiency of the rear interface modified CIGSs solar cell achieves 7.9% with an open circuit voltage of 565.8 mV, a short circuit current density of  $23.4 \text{ mA cm}^{-2}$ , and a fill factor of 59.5%. The possible strategies to further improve the efficiency of semitransparent CIGSs devices are 1) the introduction of NaCl pre-selenization treatment, and 2) the optimization of the Ga profile to increase the carrier diffusion length.

### 4. Experimental Section

**ITO Back Contact Sputtering:** Soda-lime glass (SLG) substrates ( $2.5 \text{ cm} \times 2.5 \text{ cm} \times 2 \text{ mm}$ ) were sequentially cleaned with acetone, isopropanol, and deionized water for 15 min each by sonication. Subsequently, the SLG substrates were dried by  $\text{N}_2$  flow. A 400 nm ITO layer was deposited on the cleaned SLG substrates by DC-sputtering in a PRO Line PVD 75 (Kurt J. Lesker Company) thin-film deposition system.<sup>[2b,10]</sup> The ITO back contacts were subject to pre-annealing treatment at  $500^\circ\text{C}$  for 10 min in an ambient atmosphere before spin-coating the precursor solution. Previous literature has proven that the pre-annealing treatment can improve the optical transparency and carrier mobility of ITO.<sup>[2c]</sup>

**Formation of Precursor Solution:** For the preparation of Cu-In-TU-DMF solution, first 46 mmol thiourea (TU, 99%, Alfa Aesar Company) was dissolved in 18 mL N, N-Dimethylformamide (DMF, ACS, 99.8%, Sigma-Aldrich) solvent to make a clear solution after 20 min stirring. Then, 7.77 mmol CuCl (99.8%, Sigma-Aldrich) was added to this solution and stirred until CuCl was completely dissolved. Finally, 8.45 mmol  $\text{InCl}_3$  (99.8%, Sigma-Aldrich) was introduced, and a yellowish solution was obtained after overnight stirring. The solution was filtered by using a  $0.45 \mu\text{m}$  polytetrafluoroethylene filter before spin-coating. For the Cu-In-Ga-TU-DMF solution, the 8.45 mmol  $\text{InCl}_3$  was replaced by 2.53 mmol  $\text{GaCl}_3$  and 5.92 mmol  $\text{InCl}_3$  ( $\text{Ga}/(\text{Ga}+\text{In}) = 0.3$ ).

**Fabrication of CIGSs Absorbers:** The Cu-In-Ga-TU-DMF solution was spin-coated onto the ITO back contact with a speed of 1500 rpm for 60 s, and the wet film was immediately annealed on a hot plate at  $350^\circ\text{C}$  for 2 min and moved to a ceramic plate for cooling down naturally. The spin-coating/annealing steps were repeated eight times to obtain a final absorber thickness of 730 nm. Subsequently, the as-obtained precursor films were selenized in a quartz tube furnace under a selenium atmosphere at  $350^\circ\text{C}$  for 20 min and at  $520^\circ\text{C}$  for 20 min before cooling down naturally. It should be noted that the quartz tube was evacuated and filled with argon three times before heating. This reference CIGSs absorber is referred to as R-CIGSs. For the CIGSs absorber with an interface modification treatment (named T-CIGSs), the first layer was replaced by the Cu-In-TU-DMF solution (without Ga). The other seven layers were spin-coated with Cu-In-Ga-TU-DMF solution.

**Fabrication of CIGSs Photovoltaic Devices:** 10% KCN solution was utilized to etch the CIGSs absorbers for 3 min to remove  $\text{Cu}_{2-x}(\text{S,Se})$  and excessive Se. Then, an 80 nm thick CdS buffer was grown onto the CIGSs absorbers by a chemical bath deposition process. An 80 nm i-ZnO and a 300 nm Al:ZnO layer were fabricated by RF-sputtering. Ni/Al top grids were deposited by thermal evaporation. The active area of each CIGSs solar cell was  $0.5 \text{ cm}^2$  defined by mechanical scribing. No antireflection coating layer was applied.

**Characterization:** The composition profiles of the CIGSSe absorbers were measured by glow discharge optical emission spectroscopy (GD-OES) using a Spectruma GDA 650 HR analyzer. For these measurements, the CdS buffer layer, the i-ZnO/AZO window layer, and the Ni/Al grid were removed from the solar cells used for electrical characterization. Morphological characterization was carried out using a JEOL JSM-7500F scanning electron microscope (SEM). The current density-voltage ( $J$ - $V$ ) curves were recorded under standard test conditions (AM1.5G; 100 mW cm<sup>-2</sup>; 25 °C) by a WACOM sun-simulator containing both a Xenon and a Halogen lamp. The external quantum efficiency (EQE) was measured by a home-built system applying calibrated Si and Ge diodes as references. The capacitance-voltage ( $C$ - $V$ ) curves were taken under dark conditions with a BK PRECISION Model 895 operating at 100 kHz with a 5 mV testing signal. In addition, the temperature-dependent current density-voltage measurements were carried out in an enclosed liquid helium cryostat, with the temperature sensor mounted atop the sample.

## Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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## Conflict of Interest

The authors declare no conflict of interest.

## Data Availability Statement

The data that support the findings of this study are available from the corresponding author upon reasonable request.

## Keywords

back interface modification, ITO back contact, pre-annealing treatment, solution process, submicron CIGSSe

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