

BRIEF REPORT | MARCH 16 2006

Device for *in situ* cleaving of hard crystals

M. Schmid; A. Renner; F. J. Giessibl



Rev Sci Instrum 77, 036101 (2006)

<https://doi.org/10.1063/1.2166670>



CrossMark

Articles You May Be Interested In

On-board sample cleaver

Rev Sci Instrum (July 2007)

The development of medical plier design with bending and cutting-mixed functions

AIP Conference Proceedings (April 2019)

A Crystal Cleaver and Electron Analyzer Assembly for Photoemission Studies on Vacuum Cleaved Crystals

Rev Sci Instrum (November 2003)



Time to get excited.
Lock-in Amplifiers – from DC to 8.5 GHz

[Find out more](#)

Device for *in situ* cleaving of hard crystals

M. Schmid,^{a)} A. Renner, and F. J. Giessibl

Universität Augsburg, Institute of Physics, Electronic Correlations and Magnetism, Experimentalphysik VI, Universitätsstrasse 1, D-86135 Augsburg, Germany

(Received 30 May 2005; accepted 22 November 2005; published online 16 March 2006)

Cleaving crystals in a vacuum chamber is a simple method for obtaining atomically flat and clean surfaces for materials with a preferential cleaving plane. Most *in situ* cleavers use parallel cutting edges that are applied from two sides on the sample. We found in ambient experiments that diagonal cutting pliers, where the cleavage force is introduced in a single point instead of a line, work very well also for hard materials. Here, we incorporate the diagonal cutting plier principle in a design compatible with ultrahigh-vacuum requirements. We show optical microscopy (millimeter scale) and atomic force microscopy (atomic scale) images of NiO(001) surfaces cleaved with this device. © 2006 American Institute of Physics. [DOI: 10.1063/1.2166670]

I. INTRODUCTION

Surface science relies on the availability of atomically clean and well-defined surfaces. Cleaving a crystal in an ultrahigh-vacuum environment is a simple means to provide clean and atomically flat surfaces. Existing implementations of cleavers use a spring-loaded blade that moves towards an anvil¹⁻³ with parallel edges, an anvil with one blade that presses against the sample that is to be cleaved,⁴⁻⁶ or a device that pushes the sample against an obstruction.⁷⁻⁹ Other techniques use one blade that is introduced from one side of

the vacuum chamber with a wobble-stick-type feedthrough hitting a sample that is countered by a fixed or movable anvil.¹⁰ Cleaving crystals *in situ* is relatively simple for soft materials, such as alkali halides. However, cleaving hard materials as NiO is more difficult. We could successfully cleave a strip cut from a NiO wafer with a cross section of roughly $2 \times 0.6 \text{ mm}^2$ with the techniques described in Refs. 7-9. However, in particular, on hard samples, the sample areas close to the crystal boundaries show very poor surface quality and it is desirable to provide cleavage faces with greater

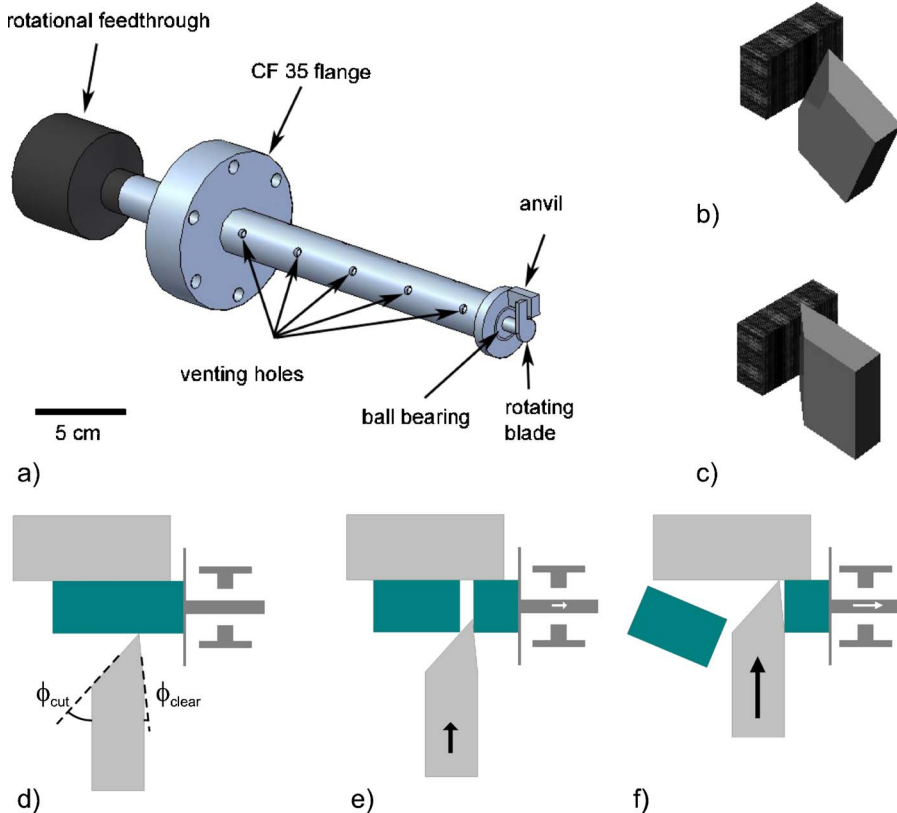


FIG. 1. (Color online) (a) Perspective view of the single-flange cleaver. It consists essentially of three parts: a rotary feedthrough that connects to an axle holding the cleavage knife and a tube with venting holds that has the anvil welded to it. (b) Cleaving a crystal using the wire cutter principle results in a well-defined point where the cleave is initiated. In contrast to a cleaver where the blade is applied parallel to the side faces of the crystal sample to be cleaved (c), the wire cutter principle does not require perfect alignment between the cutting edge and the intended cleavage direction. (d) Schematic view of the blade with cutting angle ϕ_{cut} and clearance angle ϕ_{clear} in the initial phase of cleavage. In our setup, $\phi_{\text{cut}} \approx 42^\circ$ and $\phi_{\text{clear}} \approx -6^\circ$. (e) and (f) The negative clearance angle ensures that the cleavage plane remains unscathed when the blade slide over the sample surface after the cleave (see also online movies). The sample holder is movable along a line perpendicular to the cleavage plane, enabling the sample to move backwards [white arrow in (e) and (f)].

^{a)}Electronic mail: martina.schmid@physik.uni-augsburg.de

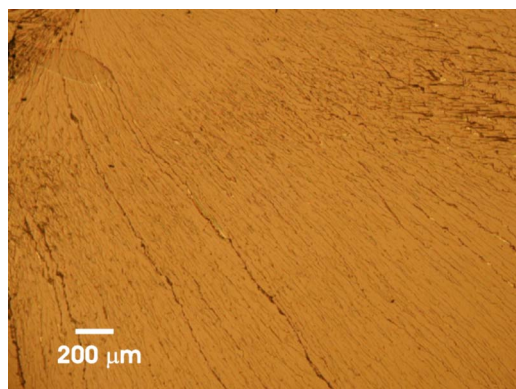


FIG. 2. (Color online) Optical microscopic view of the cleaved NiO(001) surface. Cleavage was initiated on the top left corner of the sample. The central region of the cleavage plane has a rather good surface quality, while the sections close to the boundaries are more rugged and are sometimes covered with debris.

lateral dimensions to obtain good quality surface areas. We found in ambient experiments that cleaving NiO with a razor blade that touches the sample along a line is rather difficult, while cleaving it with a wire cutter is simple and requires little force even for large cross sections. In a wire cutter, the cleavage force is introduced in a single spot. This highly localized stress field is known to facilitate cleaving.¹¹ We therefore aimed to incorporate this principle in a vacuum compatible form, shown in the next section.

II. EXPERIMENTAL IMPLEMENTATION

ur cleaver [see Fig. 1(a)] sits on a single CF 35 flange that holds a rotary feedthrough capable of transmitting a torque of 10 N m mounted on a CF 16 flange. The rotary feedthrough connects to an axle that has the cleavage knife mounted to it at its end. The CF 35 flange has a pipe with venting holes welded to it, holding an anvil at its end, and housing a ball bearing that supports the axle. Because the knife edge is not parallel to the surface when the crystal is not cleaved yet, the cleavage force is applied at a well-defined point [Fig. 1(b)], facilitating the cleavage process and usually resulting in fairly flat cleavage planes. When the knife edge is touching the crystal along its whole length, as done in many previous cleavage designs, the cleavage can start at multiple points that are on different parallel crystal planes [Fig. 1(c)]. The rotating blade and the steady anvil resemble the two cutting blades of a wire cutter. In the present cleaver, the blade is made of stainless steel, but it could also be manufactured from hardened steel or other hard materials such as tungsten carbide. The blade angles are chosen such that once the cleave is initiated, the blade pushes the sample backwards so that the blade does not scratch over the freshly cleaved surface [Fig. 1(d)–1(f)]. The maximum force that can be applied to the initial point of contact between knife and sample is given by the length of the arm and the torque of the rotary feedthrough. In our setup, it is approximately 1 kN.

III. RESULTS

Figure 2 shows an optical microscopy image of a typical

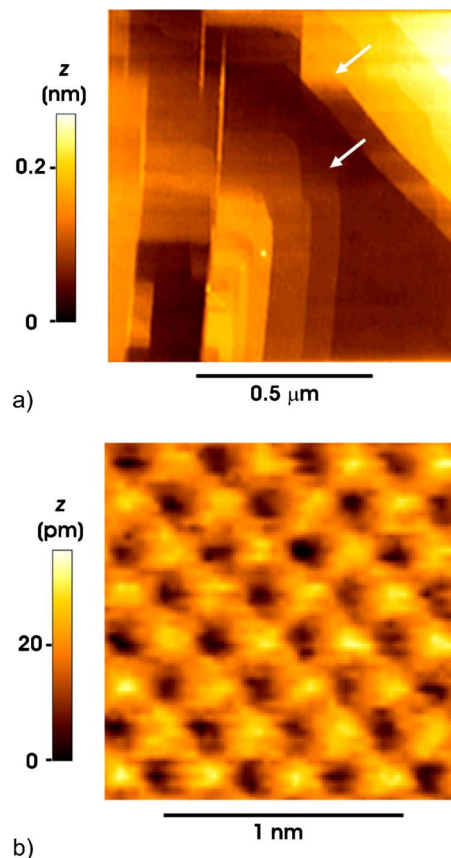


FIG. 3. (Color online) Atomic force microscopy images of the cleaved NiO(001) surface. NiO(001) has a rocksalt structure with a cubic lattice constant of $a_0=417$ pm and natural step heights of integer multiples of $a_0/2$. (a) Image of size $1\ \mu\text{m} \times 1\ \mu\text{m}$, showing atomic steps with heights of $a_0/2$ and a_0 . At the top, the NiO crystal is 3 unit cells higher at the right edge than at the left, and at the bottom, the left edge is 3 unit cells higher than the right one. The misorientation angle of the actual cleavage plane with respect to the ideal (001) plane is thus on the order of $3\ a_0/1\ \mu\text{m}\ \text{rad}=0.07^\circ$. The image shows that the (001) surfaces are not ideal - a few screw dislocations are present (arrows). (b) Atomic resolution image (size $1.5\ \text{nm} \times 1.5\ \text{nm}$). Images of this quality could only be obtained on surfaces that are flat and free of debris for fairly large areas. The larger the area of a cleaved surface, the more likely it is possible to find such good surface regions.

cleavage plane. The steplines clearly merge into the point where the initial cleaving force was applied. The cleavage process is shown in real time for soft (KBr) and hard (NiO) materials by two movies.¹² The advantage of a large cleavage area is that high-quality surface areas are more likely to be found. In most experiments, it is not possible to obtain atomic resolution over the whole surface area (see caption in Fig. 2). Debris on surfaces is especially harmful for scanning probe microscopy studies, because the radii of the probe tips are often large and even small pieces of debris on otherwise perfectly flat and clean surfaces can prevent the tip apex from reaching the flat surface.

With the cleaver shown in Fig. 1, we could easily cleave cross sections on the order of $2 \times 4\ \text{mm}^2$ and we could find surfaces that are clean enough to allow atomic resolution by atomic force microscopy (AFM) in approximately nine out of ten cleavage trials. Figure 3 shows a typical atomic force microscopy image of an *in situ* cleaved NiO(001) surface that was produced with this device.

Because the cleaver can be mounted on a single flange, it is very compact. As it uses only a single rotary feedthrough and few other parts, it is easy to build and quite cost effective.

ACKNOWLEDGMENTS

The authors thank Jochen Mannhart for support and useful suggestions, Marilyn Gleyzes for assistance with preparing the mechanical drawings, Reiner Pätzold for machining the second version of the cleaver, and Michael Reichling for helpful comments. This work is supported by the Bundesministerium für Bildung und Forschung (Project No. EKM13N6918).

¹C. A. Pela, J. X. De Oliveira, and Z. P. De Arguello, *Rev. Sci. Instrum.* **44**, 1406 (1973).

²A. P. Janssen and A. Chambers, *J. Phys. E* **7**, 425 (1974).

³T. Angot, J. Suzanne, and J. Y. Hoarau, *Rev. Sci. Instrum.* **62**, 1865 (1991).

⁴B. Dupoisson, P. Dumas, A. Steinbrunn, and J. C. Colson, *J. Phys. E* **9**, 266 (1976).

⁵R. Carr, *Rev. Sci. Instrum.* **59**, 989 (1988).

⁶J. T. Yates, *Experimental Innovations in Surface Science* (Springer, Berlin, 1998).

⁷F. J. Giessibl, Ph.D. thesis, Ludwig-Maximilians-Universität München, Germany, 1991.

⁸M. Otha, Y. Sugawara, S. Morita, N. Nagaoka, S. Mishima, and T. Okada, *J. Vac. Sci. Technol. B* **12**, 1705 (1994).

⁹Y. -C. Kim, M. J. Nopwawowski, and D. N. Seidmann, *Rev. Sci. Instrum.* **67**, 1992 (1996).

¹⁰M. Reichling (private communication).

¹¹M. E. Eberhart, *Why Things Break* (Harmony Books, New York, 2003).

¹²See EPAPS Document No. E-RSINAK-77-209602 for the movies illustrating the cleavage process. This document can be reached through a direct link in the online article's HTML reference section or via the EPAPS homepage (<http://www.aip.org/pubservs/epaps.html>).