

# A Numerical Solution Method for an Infinitesimal Elasto-Plastic Cosserat Model

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# A micropolar extension to infinitesimal elasticity

- ▶ We present a geometrically linear generalized continua of Cosserat micropolar type in the elasto-plastic case.
- ▶ We postulate independent infinitesimal microrotations of the material. Thus, as a consequence of balance of angular momentum, Cauchy stresses  $\sigma$  are not symmetric any more.
- ▶ Cosserat effects regularize the mesh size dependence of localization computations where shear failure mechanisms play a dominant role.
- ▶ We restrict Cosserat microrotations to the elastic response of the material. Inelasticity is formulated as in Prandtl-Reuß plasticity. The elasto-plastic Cosserat problem is well-posed (Neff/Chełmiński Appl.Math.Opti06, PRSE05).

# Infinitesimal time continuous Cosserat Plasticity

Let  $\Omega \subset \mathbb{R}^3$  be the reference configuration, and let  $\Gamma_D \cup \Gamma_N = \partial\Omega$  be a decomposition of the boundary.

We consider infinitesimal microrotations  $\bar{A} \in \mathfrak{so}(3) := \{\bar{B} \in \mathbf{R}^{3,3} : \bar{B}^T = -\bar{B}\}$ , and we define the symmetric bilinear form

$$\begin{aligned} a((\mathbf{u}, \bar{A}, \varepsilon_p), (\mathbf{v}, \bar{B}, \eta)) = & \\ 2\mu \int_{\Omega} (\operatorname{sym}(D\mathbf{u} - \varepsilon_p) : \operatorname{sym}(D\mathbf{v} - \eta)) \, d\mathbf{x} + \lambda \int_{\Omega} \operatorname{tr} D\mathbf{u} \cdot \operatorname{tr} D\mathbf{v} \, d\mathbf{x} \\ + 2\mu_c \int_{\Omega} (\operatorname{skew}(D\mathbf{u} - \bar{A}) : \operatorname{skew}(D\mathbf{v} - \bar{B})) \, d\mathbf{x} + 2\mu L_c^2 \int_{\Omega} D\bar{A} : D\bar{B} \, d\mathbf{x}, \end{aligned}$$

where  $\mu_c$  is the Cosserat couple modulus and  $L_c$  the internal length scale.

Here, no physical interpretation of Cosserat parameters!

The goal is regularization through elastic size effect.

Furthermore, we have the convex functional

$$j(\varepsilon_p) = \int_{\Omega} K_0 |\varepsilon_p| d\mathbf{x} ,$$

(with  $\varepsilon_p \in \{\eta \in \mathbf{R}^{d,d} : \eta^T = \eta, \text{tr } \eta = 0\}$ ), and the load functional

$$\ell(t, \mathbf{v}) = \int_{\Omega} \mathbf{b}(t) \cdot \mathbf{v} d\mathbf{x} + \int_{\Gamma_N} \mathbf{t}_N(t) \cdot \mathbf{v} d\mathbf{a} .$$

Quasi-static infinitesimal Cosserat plasticity is characterized by the variational inequality

$$a \left( (\mathbf{u}, \bar{\mathbf{A}}, \varepsilon_p), (\mathbf{v}, \bar{\mathbf{B}}, \eta) - (\dot{\mathbf{u}}, \dot{\bar{\mathbf{A}}}, \dot{\varepsilon}_p) \right) + j(\eta) - j(\dot{\varepsilon}_p) \geq \ell(\mathbf{v} - \dot{\mathbf{u}}) ,$$

for all  $(\mathbf{v}, \bar{\mathbf{B}}, \eta) \in \mathbf{V} \times W \times \mathbf{E} ,$

subject to boundary conditions and given material history  $\varepsilon_p(0) = \varepsilon_p^0$  as initial value, where  $\mathbf{V} \times W \times \mathbf{E}$  is a suitable function space.

# Infinitesimal Elasto-Plastic Cosserat Model - Equations

We want to determine

displacements

$$\mathbf{u}: \bar{\Omega} \times [0, T] \longrightarrow \mathbb{R}^3,$$

infinitesimal micro-rotations

$$\bar{\mathbf{A}}: \Omega \times [0, T] \longrightarrow \mathfrak{so}(3),$$

*non-symmetric* stresses

$$\boldsymbol{\sigma}: \Omega \times [0, T] \longrightarrow \mathbb{R}^{3,3},$$

*symmetric* plastic strains

$$\boldsymbol{\varepsilon}_p: \Omega \times [0, T] \longrightarrow \text{Sym}(3) \text{ with } \boldsymbol{\varepsilon}_p(0) = \mathbf{0},$$

and a plastic multiplier

$$\Lambda: \Omega \times [0, T] \longrightarrow \mathbb{R},$$

satisfying the essential boundary conditions and the equilibrium equations

$$-\operatorname{div} \boldsymbol{\sigma}(\mathbf{x}, t) = \mathbf{b}(\mathbf{x}, t), \quad (\mathbf{x}, t) \in \Omega \times [0, T],$$

$$\boldsymbol{\sigma}(\mathbf{x}, t) \mathbf{n}(\mathbf{x}) = \mathbf{t}_N(\mathbf{x}, t), \quad (\mathbf{x}, t) \in \Gamma_N \times [0, T],$$

$$-\mu L_c^2 \Delta \bar{\mathbf{A}}(\mathbf{x}, t) = \mu_c (\operatorname{skew}(D\mathbf{u}(\mathbf{x}, t)) - \bar{\mathbf{A}}(\mathbf{x}, t)), \quad (\mathbf{x}, t) \in \Omega \times [0, T],$$

$$D\bar{\mathbf{A}}(\mathbf{x}, t) \cdot \mathbf{n}(\mathbf{x}) = \mathbf{0}, \quad (\mathbf{x}, t) \in \Gamma_N \times [0, T],$$

the constitutive relation

$$\begin{aligned} \boldsymbol{\sigma}(\mathbf{x}, t) &= 2\mu (\operatorname{sym}(D\mathbf{u}(\mathbf{x}, t)) - \boldsymbol{\varepsilon}_p(\mathbf{x}, t)) + \lambda \operatorname{tr} D\mathbf{u}(\mathbf{x}, t) \cdot \mathbf{I} \\ &\quad + 2\mu_c (\operatorname{skew}(D\mathbf{u}(\mathbf{x}, t)) - \bar{\mathbf{A}}(\mathbf{x}, t)), \quad (\mathbf{x}, t) \in \Omega \times [0, T], \end{aligned}$$

# Infinitesimal Elasto-Plastic Cosserat Model - Equations

the complementary conditions for the yield criterion

$$\Lambda(\mathbf{x}, t)\phi(T_E(\mathbf{x}, t)) = 0, \quad \Lambda(\mathbf{x}, t) \geq 0, \quad \phi(T_E(\mathbf{x}, t)) \leq 0, \quad (\mathbf{x}, t) \in \Omega \times [0, T].$$

and the flow rule

$$\frac{d}{dt}\varepsilon_p(\mathbf{x}, t) = \Lambda(\mathbf{x}, t)D\phi(T_E(\mathbf{x}, t)), \quad (\mathbf{x}, t) \in \Omega \times [0, T],$$

depending on  $T_E(\mathbf{x}, t) = 2\mu(\text{sym}(D\mathbf{u}(\mathbf{x}, t)) - \varepsilon_p(\mathbf{x}, t))$ .

For given material history  $\varepsilon_p(t)$  at fixed time  $t$ , the displacement and the micro-rotations are determined by minimizing the total elastic energy

$$\mathcal{I}(\mathbf{u}, \bar{\mathbf{A}}, \varepsilon_p) = \mathcal{E}(\varepsilon(\mathbf{u}), \bar{\mathbf{A}}, \varepsilon_p) - \ell(t, \mathbf{u}),$$

$$\begin{aligned} \text{with } \mathcal{E}(\varepsilon, \bar{\mathbf{A}}, \varepsilon_p) &= \mu \int_{\Omega} |\text{sym}(\varepsilon) - \varepsilon_p|^2 d\mathbf{x} + \frac{\lambda}{2} \int_{\Omega} \text{tr}(\varepsilon)^2 d\mathbf{x} \\ &\quad + \mu_c \int_{\Omega} |\text{skew}(\varepsilon) - \bar{\mathbf{A}}|^2 d\mathbf{x} + \mu L_c^2 \int_{\Omega} |D\bar{\mathbf{A}}|^2 d\mathbf{x}. \end{aligned}$$

# Discrete formulation of the Elasto-Plastic Model

Let  $\mathbf{V}_h \times W_h$  be a finite element space with  $\mathbf{v}_h = \mathbf{0}$  and  $\bar{\mathbf{B}}_h = 0$  on  $\Gamma_D$ .

The model of incremental infinitesimal plasticity is obtained by a decomposition  $0 = t_0 < t_1 < \dots < t_N = T$  of the time interval and backward Euler scheme.

**Lemma:**

The fully discrete elasto-plastic problem is equivalent to the following nonlinear weak problem. For given  $\varepsilon_p^{n-1}$  find  $(\mathbf{u}^n, \bar{\mathbf{A}}^n) \in \mathbf{V}_h \times W_h$  such that

$$\begin{aligned} & \int_{\Omega} P_{\mathbf{K}}(2\mu(\text{sym}(D\mathbf{u}_h^n) - \varepsilon_p^{n-1})) : D\mathbf{v}_h \, d\mathbf{x} + \lambda \int_{\Omega} \text{tr } D\mathbf{u}_h^n \cdot \text{tr } D\mathbf{v}_h \, d\mathbf{x} \\ & + 2\mu_c \int_{\Omega} (\text{skew}(D\mathbf{u}_h^n) - \bar{\mathbf{A}}_h^n) : D\mathbf{v}_h \, d\mathbf{x} = \ell(t_n, \mathbf{v}_h), \quad \mathbf{v}_h \in \mathbf{V}_h, \end{aligned}$$

$$\mu L_c^2 \int_{\Omega} D\bar{\mathbf{A}}_h^n \cdot D\bar{\mathbf{B}}_h \, d\mathbf{x} = \mu_c \int_{\Omega} (\text{skew}(D\mathbf{u}_h^n) - \bar{\mathbf{A}}_h^n) : \bar{\mathbf{B}}_h \, d\mathbf{x}, \quad \bar{\mathbf{B}}_h \in W_h,$$

with the orthogonal projection  $P_{\mathbf{K}}(\theta) = \theta - \max \{0, |\text{dev}(\theta)| - K_0\} \frac{\text{dev}(\theta)}{|\text{dev}(\theta)|}$  on the elastic domain  $\mathbf{K} := \{\boldsymbol{\tau} \in \mathbf{R}^{3,3} : \boldsymbol{\tau}^T = \boldsymbol{\tau}, |\text{dev } \boldsymbol{\tau}| \leq K_0\}$  of the von Mises flow rule.

# Variational Formulation of the discrete problem

**Lemma:**

Any minimizer  $(\mathbf{u}_h^n, \bar{\mathbf{A}}_h^n) \in \mathbf{V}_h \times W_h$  of the functional

$$\mathcal{I}_{\text{incr}}^n(\mathbf{u}_h, \bar{\mathbf{A}}_h) = \mathcal{E}_{\text{incr}}(D\mathbf{u}_h, \bar{\mathbf{A}}_h, \varepsilon_p^{n-1}) - \ell(t_n, \mathbf{u}_h)$$

solves the nonlinear variational update problem. Here  $\mathcal{E}_{\text{incr}}$  denotes the free energy of the incremental update problem defined by

$$\begin{aligned} \mathcal{E}_{\text{incr}}(D\mathbf{u}, \bar{\mathbf{A}}, \varepsilon_p) &= \frac{1}{2\mu} \int_{\Omega} \psi_{\mathbf{K}}(2\mu(\text{sym}(D\mathbf{u}) - \varepsilon_p)) d\mathbf{x} + \frac{\lambda}{2} \int_{\Omega} \text{tr}(D\mathbf{u})^2 d\mathbf{x} \\ &\quad + \mu_c \int_{\Omega} |\text{skew}(D\mathbf{u}) - \bar{\mathbf{A}}|^2 d\mathbf{x} + \mu L_c^2 \int_{\Omega} |D\bar{\mathbf{A}}|^2 d\mathbf{x}, \end{aligned}$$

$$\psi_{\mathbf{K}}(\theta) = \begin{cases} \frac{1}{2} |\theta|^2 & |\text{dev}(\theta)| \leq K_0, \\ \frac{1}{2} \left( \frac{1}{d} \text{tr}(\theta)^2 + 2K_0 |\text{dev}(\theta)| - K_0^2 \right) & |\text{dev}(\theta)| > K_0. \end{cases}$$

If  $\varepsilon_p^{n-1} = 0$  and  $\mu_c = 0 \rightarrow$  classical Hencky-Problem.

# The FEM convergence

**Theorem:**

We have

$$\|(\mathbf{u} - \mathbf{u}_h, \bar{\mathbf{A}} - \bar{\mathbf{A}}_h)\|_{\mathbf{V} \times \mathbf{W}} \leq \frac{C}{\mu_c} \inf_{(\mathbf{v}_h, \bar{\mathbf{B}}_h) \in \mathbf{V}_h \times \mathbf{W}_h} \|(\mathbf{u} - \mathbf{v}_h, \bar{\mathbf{A}} - \bar{\mathbf{B}}_h)\|_{\mathbf{V} \times \mathbf{W}}.$$

$C$  is independent of  $\mu_c \in (0, \mu]$ .

If the analytical solution  $u$  is  $H^2$ -smooth then

$$\inf_{(\mathbf{v}_h, \bar{\mathbf{B}}_h) \in \mathbf{V}_h \times \mathbf{W}_h} \|(\mathbf{u} - \mathbf{v}_h, \bar{\mathbf{A}} - \bar{\mathbf{B}}_h)\|_{\mathbf{V} \times \mathbf{W}} \leq C h (\|u\|_{H^2(\Omega)} + \|\bar{\mathbf{A}}\|_{H^2(\Omega)}) .$$

Neff/Knees: Cosserat update problem admits unique global  $H^2$ -solutions!

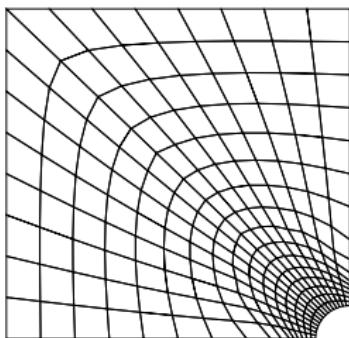
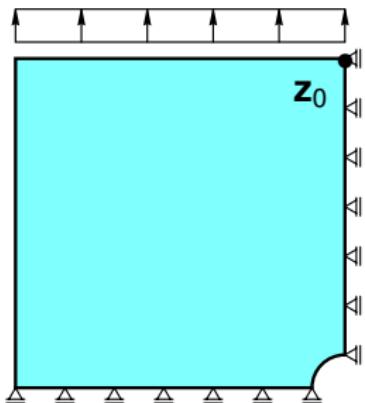
Idea: balance  $h$  against  $\mu_c$ .

## Plate with a hole

Let  $\Omega = (0, 10) \times (0, 10) \setminus B_1(10, 0)$ . We use Q1 discretization and present results for 198147 unknowns on uniform refinement level 4. We have chosen the parameters  $K_0 = 450$ ,  $\lambda = 110743.8$ ,  $\mu = 80193.8$  and  $L_c = 0.020833$ .

And apply traction force by Neumann boundary condition according to:

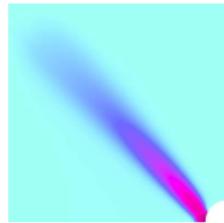
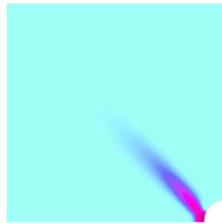
$$\ell(t, v) = 100t \int_0^{10} \mathbf{v}(x_1, 10) dx_1.$$



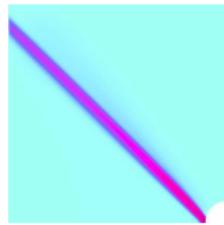
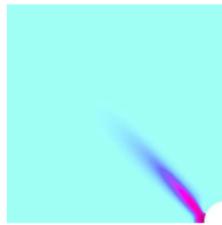
Geometry, boundary conditions and coarse mesh.

# Numerical Experiment with M++

Cosserat Model ( $\mu_c = \mu$ ) : Effective plastic strain



Prandtl-Reuß ( $\mu_c = 0$ ) : Effective plastic strain

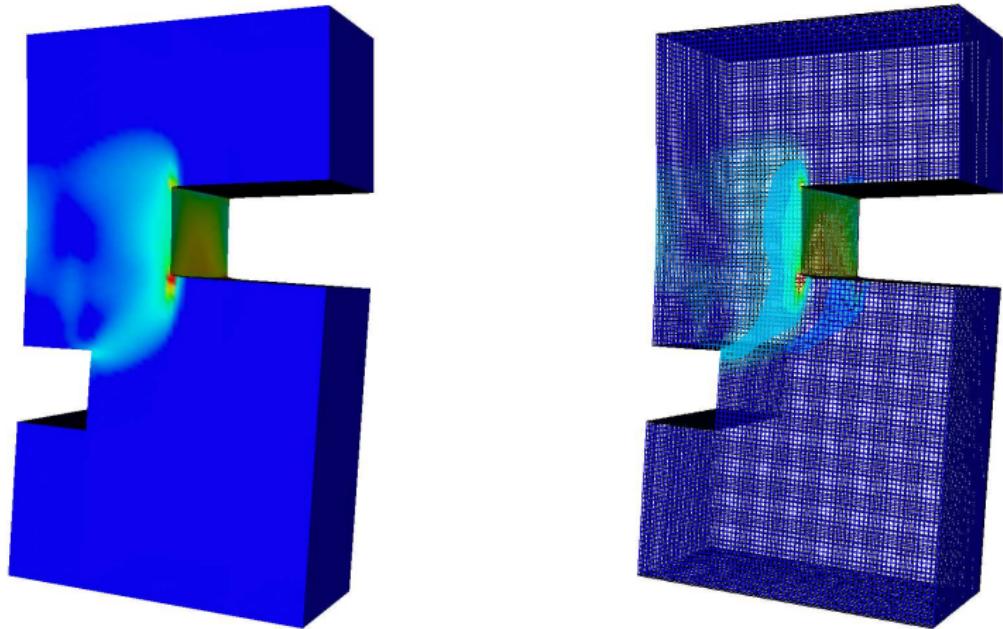


$t = 4.00$

$t = 4.40$

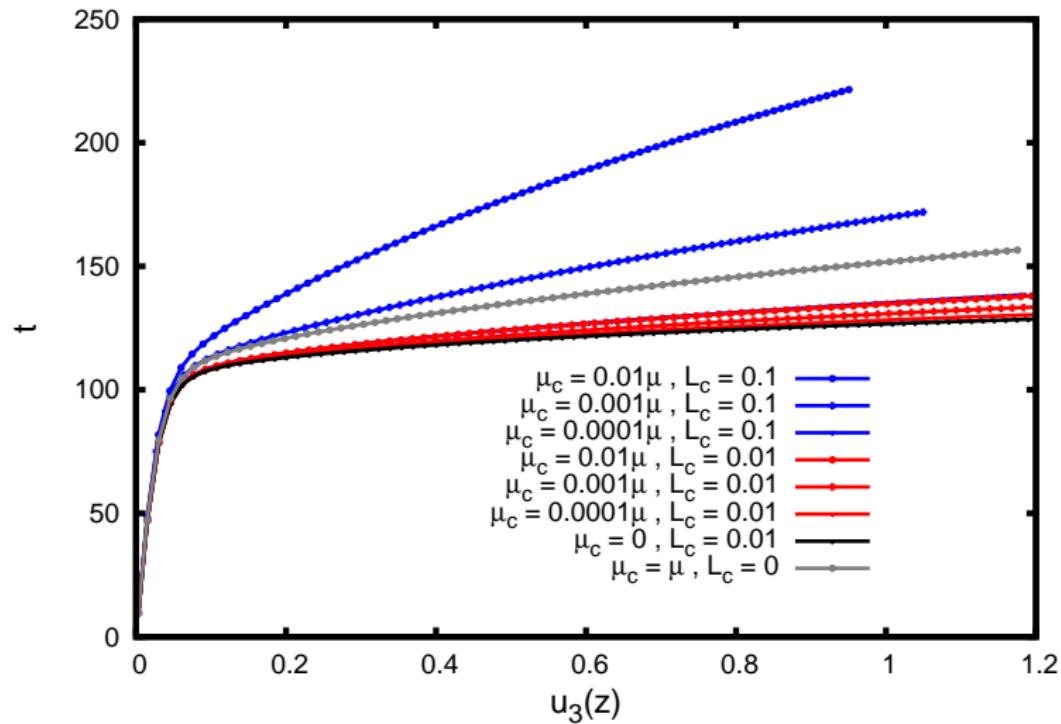
$t = 4.69$

## Notched cube - a test configuration in 3D



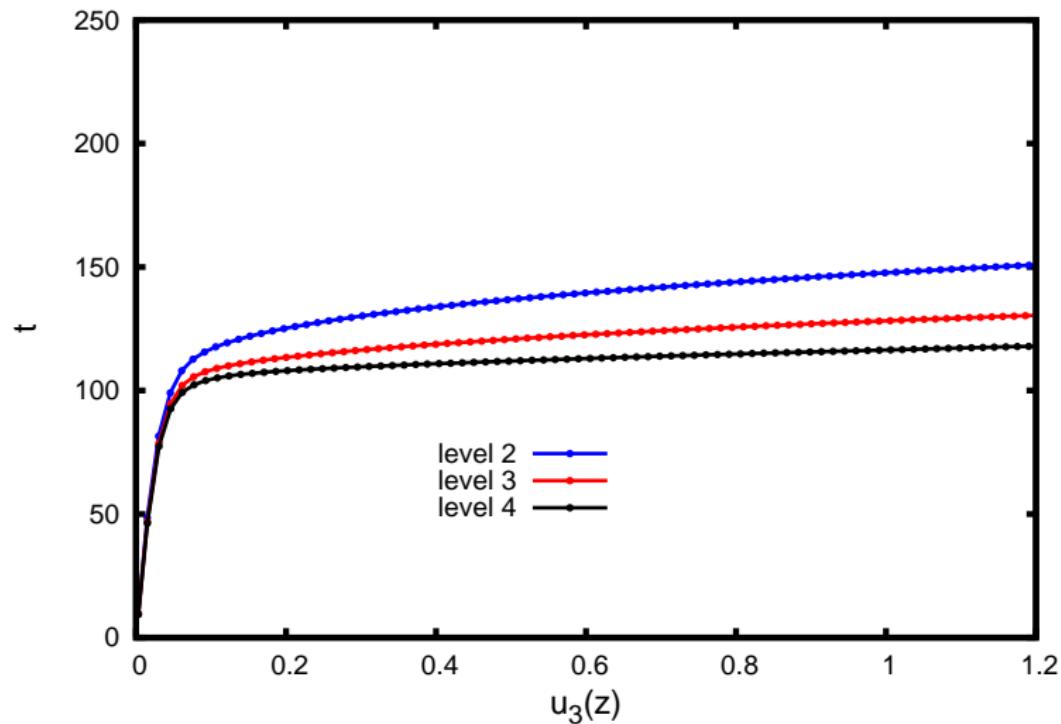
For the linear subproblem in each Newton step,  
we use a parallel multilevel GMRES algorithm.

# Numerical Experiment with M++



Load-displacement curve for notched cube on refinement level 3.  
Here, we use 174.727 dof for displacement and microrotation.

# Numerical Experiment with M++



Here, we compute up to 1.311.751 dof on refinement level 2, 3 and 4 ( $\mu_c = 0.0001\mu$ ,  $L_c = 0.01$ ). We observe about linear convergence in  $h$ .

## Summary and Outlook

- ▶ The Elasto-Plastic Cosserat Model with pure Dirichlet data is well-posed: unique solution globally in time.
- ▶ The discrete update problem admits global  $H^2$ -solutions.
- ▶ For linear Lagrange elements, we have linear convergence in  $h$ .
- ▶ The Elasto-Plastic Cosserat Model is a regularization for classical perfect plasticity (shear failure mechanisms).
- ▶ Future work will be the analysis and robust implementation of geometrically nonlinear elasto-plastic Cosserat Models.

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