

Weakly symmetric stress equilibration in computational solid mechanics

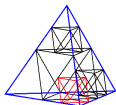
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Overview

Stress Equilibration: Basic Idea

Stress Equilibration: The Role of Weak Symmetry

Weakly Symmetric Stress Equilibration: Upper Bound

Weakly Symmetric Stress Equilibration: Lower Bound

Extensions to Nonlinear Deformation Models

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Stress Equilibration: Basic Idea

The Linear Elasticity Model

$$\varepsilon(\mathbf{v}) := \frac{\nabla \mathbf{v} + (\nabla \mathbf{v})^T}{2} = \nabla \mathbf{v} - \frac{\nabla \mathbf{v} - (\nabla \mathbf{v})^T}{2} =: \nabla \mathbf{v} - \text{as } \nabla \mathbf{v}$$

Determine $\mathbf{u} \in H_{\Gamma_D}^1(\Omega)^d$, $d = 2, 3$, such that

$$2\mu (\varepsilon(\mathbf{u}), \varepsilon(\mathbf{v}))_{L^2(\Omega)} + \lambda (\text{tr } \varepsilon(\mathbf{u}), \text{tr } \varepsilon(\mathbf{v}))_{L^2(\Omega)} = (\mathbf{f}, \mathbf{v})_{L^2(\Omega)} + \langle \mathbf{t}, \mathbf{v} \rangle_{\Gamma_N}$$

holds for all $\mathbf{v} \in H_{\Gamma_D}^1(\Omega)^d$

Scaling: $\mu \approx 1$ (by appropriate choice of units)

Incompressibility: $\lambda \rightarrow \infty$, new variable (pressure): $p = \lambda \text{tr } \varepsilon(\mathbf{u}) = \lambda \text{div } \mathbf{u}$

Treatment of (near-)incompressibility: Fleuriann Bertrand on Monday!

Finite element space $\mathbf{V}_h \subset H_{\Gamma_D}^1(\Omega)^d$

Determine $\mathbf{u}_h \in \mathbf{V}_h$ such that

$$2\mu (\varepsilon(\mathbf{u}_h), \varepsilon(\mathbf{v}_h))_{L^2(\Omega)} + \lambda (\text{tr } \varepsilon(\mathbf{u}_h), \text{tr } \varepsilon(\mathbf{v}_h))_{L^2(\Omega)} = (\mathbf{f}, \mathbf{v}_h)_{L^2(\Omega)} + \langle \mathbf{t}, \mathbf{v}_h \rangle_{L^2(\Gamma_N)}$$

holds for all $\mathbf{v}_h \in \mathbf{V}_h$

Stress Equilibration: Basic Idea

Raviart-Thomas Finite Element Spaces

The stress tensor $\boldsymbol{\sigma} = 2\mu\boldsymbol{\varepsilon}(\mathbf{u}) + \lambda(\operatorname{div} \mathbf{u}) \mathbf{I}$ satisfies

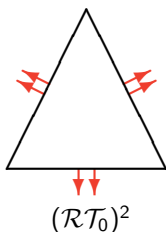
$$\operatorname{div} \boldsymbol{\sigma} + \mathbf{f} = \mathbf{0} \text{ in } \Omega$$

$$\boldsymbol{\sigma} \cdot \mathbf{n} = \mathbf{t} \text{ on } \Gamma_N$$

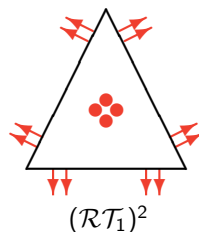
Finite element space $\boldsymbol{\Sigma}_h$ for stress approximation should be in $H(\operatorname{div}, \Omega)^d$
Raviart-Thomas space $(\mathcal{RT}_k)^d$:

$$\boldsymbol{\Sigma}_h \subset H(\operatorname{div}, \Omega)^d : \boldsymbol{\sigma}_h|_T \in \mathcal{P}_k^{d \times d}(T) + \mathcal{P}_k^d(T) \mathbf{x}^T \text{ for all } T \in \mathcal{T}_h\}$$

$k = 0$:



$k = 1$:



Stress Equilibration: Basic Idea

In general: $\boldsymbol{\sigma}(\mathbf{u}_h) = 2\mu\boldsymbol{\varepsilon}(\mathbf{u}_h) + \lambda(\operatorname{div} \mathbf{u}_h) \mathbf{I} \notin H(\operatorname{div}, \Omega)^d$

Reconstruct $\boldsymbol{\sigma}_h^R \in H(\operatorname{div}, \Omega)^d$ with $\operatorname{div} \boldsymbol{\sigma}_h^R + \mathbf{f} = \mathbf{0}$ in Ω , $\boldsymbol{\sigma}_h^R \cdot \mathbf{n} = \mathbf{t}$ on Γ_N

Flux/stress reconstruction algorithms, equilibrated fluxes/stresses:

Ern/Vohralík (2015, ...) ...

... Hannukainen/Stenberg/Vohralík (2012) ...

... Cai/Zhang (2012, ...) ...

... Braess/Schöberl (2008) ...

... Nicaise/Witowski/Wohlmuth (2008) ...

... Parés/Diez/Huerta (2006) ...

... Ainsworth/Oden (1993) ...

... Ladevéze/Leguillon (1983) ...

... Prager/Synge (1947)

Stress Equilibration: Basic Idea

Partition of unity with vertex basis functions:

$$1 \equiv \sum_{z \in \mathcal{V}_h} \phi_z$$

Vertex patch:

$$\omega_z = \bigcup \{T \in \mathcal{T}_h : z \text{ is a vertex of } T\}$$

$$\boldsymbol{\sigma}_h^R = \boldsymbol{\sigma}(\mathbf{u}_h) + \boldsymbol{\sigma}_h^\Delta = \boldsymbol{\sigma}(\mathbf{u}_h) + \sum_{z \in \mathcal{V}_h} \boldsymbol{\sigma}_{h,z}^\Delta \quad \text{with}$$

$$\boldsymbol{\sigma}_{h,z}^\Delta \in \boldsymbol{\Sigma}_{h,z} := \{\boldsymbol{\tau} \in L^2(\omega_z) : \boldsymbol{\tau}|_T \in RT_k(T)^d, \boldsymbol{\tau} \cdot \mathbf{n} = \mathbf{0} \text{ on } \partial\omega_z\}$$

(appropriately modified for patches with $\partial\omega_z \cap \partial\Omega \neq \emptyset$)

$$\boldsymbol{\sigma}_{h,z}^\Delta \in \boldsymbol{\Sigma}_{h,z}^\Delta \text{ s. t.}$$

$$(\operatorname{div} \boldsymbol{\sigma}_{h,z}^\Delta, \mathbf{z})_T = -((\mathbf{f} + \operatorname{div} \boldsymbol{\sigma}(\mathbf{u}_h))\phi_z, \mathbf{z})_T \quad \forall \mathbf{z} \in P_k(T)^d, T \subset \omega_z$$

$$\langle \llbracket \boldsymbol{\sigma}_{h,z}^\Delta \cdot \mathbf{n} \rrbracket_S, \boldsymbol{\zeta} \rangle_S = -\langle \llbracket \boldsymbol{\sigma}(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \boldsymbol{\zeta} \rangle_S \quad \forall \boldsymbol{\zeta} \in P_k(S)^d, S \subset \omega_z$$

$$\text{ensures that } \boldsymbol{\sigma}_h^R \in \boldsymbol{\Sigma}_h \text{ and } \operatorname{div} \boldsymbol{\sigma}_h^R + \mathbf{f} = \mathbf{0}$$

Stress Equilibration: Basic Idea

$$\boldsymbol{\sigma}_{h,z}^{\Delta} \in \boldsymbol{\Sigma}_{h,z}^{\Delta} \text{ s. t.}$$

$$(\operatorname{div} \boldsymbol{\sigma}_{h,z}^{\Delta}, \mathbf{z})_T = -((\mathbf{f} + \operatorname{div} \boldsymbol{\sigma}(\mathbf{u}_h))\phi_z, \mathbf{z})_T \quad \forall \mathbf{z} \in P_k(T)^d, T \subset \omega_z$$

$$\langle \llbracket \boldsymbol{\sigma}_{h,z}^{\Delta} \cdot \mathbf{n} \rrbracket_S, \boldsymbol{\zeta} \rangle_S = -\langle \llbracket \boldsymbol{\sigma}(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \boldsymbol{\zeta} \rangle_S \quad \forall \boldsymbol{\zeta} \in P_k(S)^d, S \subset \omega_z$$

Constraints are not linearly independent since, for all constant $\mathbf{e} \in \mathbb{R}^d$:

$$\sum_{T \subset \omega_z} (\operatorname{div} \boldsymbol{\sigma}_{h,z}^{\Delta}, \mathbf{e})_T + \sum_{S \subset \omega_z} \langle \llbracket \boldsymbol{\sigma}_{h,z}^{\Delta} \cdot \mathbf{n} \rrbracket_S, \mathbf{e} \rangle_S = 0$$

Kernel of the adjoint operator: $\operatorname{span}\{\mathbf{e}_1, \dots, \mathbf{e}_d\}$

Compatibility condition: Right-hand side \perp to $\operatorname{span}\{\mathbf{e}_1, \dots, \mathbf{e}_d\}$, i.e.,

$$\sum_{T \subset \omega_z} ((\mathbf{f} + \operatorname{div} \boldsymbol{\sigma}(\mathbf{u}_h))\phi_z, \mathbf{e})_T + \sum_{S \subset \omega_z} \langle \llbracket \boldsymbol{\sigma}(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \mathbf{e} \rangle_S = 0$$

follows from $(\mathbf{f}, \phi_z \mathbf{e})_{\omega_z} - (\boldsymbol{\sigma}(\mathbf{u}_h), \boldsymbol{\varepsilon}(\phi_z \mathbf{e}))_{\omega_z} = 0$ (since $\phi_z \mathbf{e} \in \mathbf{V}_h$)

Stress Equilibration: Basic Idea

Concentrate on stress symmetry and ignore the incompressibility issue!

$$\boldsymbol{\sigma}(\mathbf{u}_h) = 2\mu\boldsymbol{\varepsilon}(\mathbf{u}_h) + \lambda(\operatorname{div} \mathbf{u}_h) \mathbf{I} =: \mathcal{C}\boldsymbol{\varepsilon}(\mathbf{u}_h)$$

$$\implies \boldsymbol{\varepsilon}(\mathbf{u}_h) = \mathcal{C}^{-1}\boldsymbol{\sigma}(\mathbf{u}_h) = \frac{1}{2\mu} \left(\boldsymbol{\sigma}(\mathbf{u}_h) - \frac{\lambda}{d\lambda + 2\mu} (\operatorname{tr} \boldsymbol{\sigma}(\mathbf{u}_h)) \mathbf{I} \right)$$

$$\boldsymbol{\sigma}_h^R \in \boldsymbol{\Sigma}_h \text{ with } \operatorname{div} \boldsymbol{\sigma}_h^R + \mathbf{f} = \mathbf{0}$$

$$\begin{aligned} \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}(\mathbf{u}_h)\|_{\mathcal{C}^{-1}}^2 &= \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma} + \boldsymbol{\sigma} - \boldsymbol{\sigma}(\mathbf{u}_h)\|_{\mathcal{C}^{-1}}^2 \\ &= \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}\|_{\mathcal{C}^{-1}}^2 + \|\boldsymbol{\sigma}(\mathbf{u}) - \boldsymbol{\sigma}(\mathbf{u}_h)\|_{\mathcal{C}^{-1}}^2 \\ &\quad + 2(\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}, \mathcal{C}^{-1}(\boldsymbol{\sigma}(\mathbf{u}) - \boldsymbol{\sigma}(\mathbf{u}_h))) \\ &= \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}\|_{\mathcal{C}^{-1}}^2 + \|\boldsymbol{\varepsilon}(\mathbf{u}) - \boldsymbol{\varepsilon}(\mathbf{u}_h)\|_{\mathcal{C}}^2 \\ &\quad + 2 \underbrace{(\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}, \boldsymbol{\varepsilon}(\mathbf{u}) - \boldsymbol{\varepsilon}(\mathbf{u}_h))}_{\substack{(\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}, \nabla \mathbf{u} - \nabla \mathbf{u}_h) - (\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}, \operatorname{as} \nabla \mathbf{u} - \operatorname{as} \nabla \mathbf{u}_h) \\ = -(\operatorname{div}(\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}), \mathbf{u} - \mathbf{u}_h) - (\operatorname{as} \boldsymbol{\sigma}_h^R, \nabla \mathbf{u} - \nabla \mathbf{u}_h) \\ = \\ -(\operatorname{as} \boldsymbol{\sigma}_h^R, \nabla \mathbf{u} - \nabla \mathbf{u}_h)}} \end{aligned}$$

Stress Equilibration: Basic Idea

⇒ Upper bound for the energy norm of the error:

$$\begin{aligned}\|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|_{\mathcal{C}}^2 &\leq \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}(\mathbf{u}_h)\|_{\mathcal{C}^{-1}}^2 + 2\|\mathbf{as} \boldsymbol{\sigma}_h^R\| \|\nabla(\mathbf{u} - \mathbf{u}_h)\| \\ &\leq \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}(\mathbf{u}_h)\|_{\mathcal{C}^{-1}}^2 + 2\|\mathbf{as} \boldsymbol{\sigma}_h^R\| C_K \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\| \\ &= \|\boldsymbol{\sigma}_h^\Delta\|_{\mathcal{C}^{-1}}^2 + 2\|\mathbf{as} \boldsymbol{\sigma}_h^\Delta\| C_K \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|\end{aligned}$$

using Korn's inequality $\|\nabla(\mathbf{u} - \mathbf{u}_h)\| \leq C_K \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|$

With $\mathbf{dev} \boldsymbol{\tau} := \boldsymbol{\tau} - \frac{1}{d}(\text{tr } \boldsymbol{\tau})\mathbf{I}$:

$$\begin{aligned}\|\boldsymbol{\sigma}_h^\Delta\|_{\mathcal{C}^{-1}}^2 &= (\mathcal{C}^{-1} \boldsymbol{\sigma}_h^\Delta, \boldsymbol{\sigma}_h^\Delta) = \frac{1}{2\mu}(\mathbf{dev} \boldsymbol{\sigma}_h^\Delta + \frac{2\mu}{d(d\lambda + 2\mu)}(\text{tr } \boldsymbol{\sigma}_h^\Delta)\mathbf{I}, \boldsymbol{\sigma}_h^\Delta) \\ &= \frac{1}{2\mu}\|\mathbf{dev} \boldsymbol{\sigma}_h^\Delta\|^2 + \frac{2\mu}{d(d\lambda + 2\mu)}\|\text{tr } \boldsymbol{\sigma}_h^\Delta\|^2 \\ &\geq \frac{1}{2\mu}\|\mathbf{dev} \boldsymbol{\sigma}_h^\Delta\|^2 \geq \frac{1}{2\mu}\|\mathbf{as} \boldsymbol{\sigma}_h^\Delta\|^2\end{aligned}$$

$$\Rightarrow \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|_{\mathcal{C}}^2 \leq \|\boldsymbol{\sigma}_h^\Delta\|_{\mathcal{C}^{-1}}^2 + 2C_K \|\boldsymbol{\sigma}_h^\Delta\|_{\mathcal{C}^{-1}} \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|_{\mathcal{C}}$$

$$\Rightarrow \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|_{\mathcal{C}}^2 \leq 2(1 + 4C_K^2) \|\boldsymbol{\sigma}_h^\Delta\|_{\mathcal{C}^{-1}}^2$$

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Extensions to Nonlinear Deformation Models

Stress Equilibration: The Role of Weak Symmetry

$$\|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|_C^2 = \|\boldsymbol{\sigma}_h^\Delta\|_{C^{-1}}^2 - \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}\|_{C^{-1}}^2 + 2(\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta, \nabla(\mathbf{u} - \mathbf{u}_h))$$

What can we do with the term $(\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta, \nabla \mathbf{u} - \nabla \mathbf{u}_h)$?

$$\begin{aligned} (\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta, \nabla \mathbf{u} - \nabla \mathbf{u}_h) &\leq \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\| \|\nabla(\mathbf{u} - \mathbf{u}_h)\| \leq \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\| C_K^{\text{glob}} \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\| \\ &\leq \frac{(C_K^{\text{glob}})^2}{2\delta} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\|^2 + \frac{\delta}{2} \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|^2 \end{aligned}$$

with a **global** Korn constant C_K^{glob} depending on the **problem** (domain, boundary conditions)

RM = $\text{span}\{\mathbf{e}_1, \dots, \mathbf{e}_d, \boldsymbol{\rho}_1, \dots, \boldsymbol{\rho}_{d(d-1)/2}\}$ (rigid body modes)

Use a **local** Korn inequality instead:

$$\inf_{\boldsymbol{\rho} \in \text{RM}} \|\nabla(\mathbf{u} - \mathbf{u}_h - \boldsymbol{\rho})\|_{\omega_z} \leq C_K^{\text{loc}} \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|_{\omega_z}$$

with C_K^{loc} only dependent on the shape regularity of the triangulation
[Horgan: SIAM Review (1995)]

Stress Equilibration: The Role of Weak Symmetry

$$\nabla \rho = \mathbf{J}^d(\alpha) \text{ with}$$

$$\mathbf{J}^2(\alpha) = \begin{pmatrix} 0 & \alpha \\ -\alpha & 0 \end{pmatrix}, \quad \mathbf{J}^3(\alpha) = \begin{pmatrix} 0 & \alpha_3 & -\alpha_2 \\ -\alpha_3 & 0 & \alpha_1 \\ \alpha_2 & -\alpha_1 & 0 \end{pmatrix}$$

$$\begin{aligned} (\text{as } \sigma_h^\Delta, \nabla \mathbf{u} - \nabla \mathbf{u}_h)_{\omega_z} &= (\text{as } \sigma_h^\Delta, \nabla(\mathbf{u} - \mathbf{u}_h - \rho))_{\omega_z} \text{ for all } \rho \in \mathbf{RM} \\ \iff (\text{as } \sigma_h^\Delta, \mathbf{J}^d(\alpha))_{\omega_z} &= 0 \text{ for all } \alpha \in \mathbb{R}^{d(d-1)/2} \end{aligned}$$

Add this constraint to the local stress equilibration problem:

$$\begin{aligned} \sigma_{h,z}^\Delta &\in \Sigma_{h,z}^\Delta \text{ s. t.} \\ (\operatorname{div} \sigma_{h,z}^\Delta, \mathbf{z})_T &= -((\mathbf{f} + \operatorname{div} \sigma(\mathbf{u}_h))\phi_z, \mathbf{z})_T & \forall \mathbf{z} \in P_k(T)^d, T \subset \omega_z \\ \langle \llbracket \sigma_{h,z}^\Delta \cdot \mathbf{n} \rrbracket_S, \zeta \rangle_S &= -\langle \llbracket \sigma(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \zeta \rangle_S & \forall \zeta \in P_k(S)^d, S \subset \omega_z \\ (\text{as } \sigma_{h,z}^\Delta, \mathbf{J}^d(\alpha))_{\omega_z} &= 0 & \forall \alpha \in \mathbb{R}^{d(d-1)/2} \end{aligned}$$

Stress Equilibration: The Role of Weak Symmetry

Still well-posed and we may constrain symmetry even more:

$$\begin{aligned}\sigma_{h,z}^\Delta &\in \Sigma_{h,z}^\Delta \text{ s. t.} \\ (\operatorname{div} \sigma_{h,z}^\Delta, \mathbf{z})_T &= -((\mathbf{f} + \operatorname{div} \sigma(\mathbf{u}_h))\phi_z, \mathbf{z})_T \quad \forall \mathbf{z} \in P_k(T)^d, \quad T \subset \omega_z \\ \langle \llbracket \sigma_{h,z}^\Delta \cdot \mathbf{n} \rrbracket_S, \zeta \rangle_S &= -\langle \llbracket \sigma(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \zeta \rangle_S \quad \forall \zeta \in P_k(S)^d, \quad S \subset \omega_z \\ (\operatorname{as} \sigma_{h,z}^\Delta, \mathbf{J}^d(\gamma))_{\omega_z} &= 0 \quad \forall \gamma \in P_1(\mathcal{T}_h)|_{\omega_z} \cap H^1(\omega_z)\end{aligned}$$

Kernel of the adjoint operator associated with **RM**

Well-posedness follows from inf-sup stability of the finite element triple $RT_k(\mathcal{T}_h)/P_k(\mathcal{T}_h)$ (discont.)/ $P_k(\mathcal{T}_h) \cap H^1$ for $k \geq 1$

[Boffi/Brezzi/Fortin: *Commun. Pure Appl. Anal.* **8** (2009)]

$$\begin{aligned}\implies \forall \alpha_h &= \sum_{z \in \mathcal{V}_h} \alpha_z \phi_z \text{ with } \alpha_z \in \mathbb{R}^{d(d-1)/2} : \\ (\operatorname{as} \sigma_h^\Delta, \mathbf{J}^d(\alpha_h)) &= \sum_{z \in \mathcal{V}_h} (\operatorname{as} \sigma_h^\Delta, \mathbf{J}^d(\alpha_z) \phi_z) = \sum_{z \in \mathcal{V}_h} (\operatorname{as} \sigma_h^\Delta, \mathbf{J}^d(\alpha_z) \phi_z)_{\omega_z} = 0\end{aligned}$$

Stress Equilibration: The Role of Weak Symmetry

Lemma [Bertrand/Kober/Moldenhauer/GS (2018)]:

If $(\mathbf{as} \, \sigma_h^\Delta, \mathbf{J}^d(\alpha_h)) = 0$ for all $\alpha_h \in P_1(\mathcal{T}_h) \cap H^1(\Omega)$, then

$$|(\mathbf{as} \, \sigma_h^\Delta, \nabla(\mathbf{u} - \mathbf{u}_h))| \leq C_K^{\text{loc}} \|\mathbf{as} \, \sigma_h^\Delta\| \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|$$

holds with C_K^{loc} depending only on the shape regularity of \mathcal{T}_h .

Proof:

$$\begin{aligned} |(\mathbf{as} \, \sigma_h^\Delta, \nabla(\mathbf{u} - \mathbf{u}_h))| &= |(\mathbf{as} \, \sigma_h^\Delta, \nabla(\mathbf{u} - \mathbf{u}_h) - \mathbf{J}^d(\alpha_h))| \\ &= \left| \sum_{z \in \mathcal{V}_h} (\mathbf{as} \, \sigma_h^\Delta, (\nabla(\mathbf{u} - \mathbf{u}_h) - \mathbf{J}^d(\alpha_z)) \phi_z)_{\omega_z} \right| \\ &= \left| \sum_{z \in \mathcal{V}_h} ((\mathbf{as} \, \sigma_h^\Delta) \phi_z, \nabla(\mathbf{u} - \mathbf{u}_h) - \mathbf{J}^d(\alpha_z))_{\omega_z} \right| \\ &\leq \sum_{z \in \mathcal{V}_h} \|(\mathbf{as} \, \sigma_h^\Delta) \phi_z\|_{\omega_z} \|\nabla(\mathbf{u} - \mathbf{u}_h) - \mathbf{J}^d(\alpha_z)\|_{\omega_z} \\ &\leq \sum_{z \in \mathcal{V}_h} \|\mathbf{as} \, \sigma_h^\Delta\|_{\omega_z} \|\nabla(\mathbf{u} - \mathbf{u}_h) - \mathbf{J}^d(\alpha_z)\|_{\omega_z} \end{aligned}$$

Stress Equilibration: The Role of Weak Symmetry

Choose α_z such that

$$\|\nabla(\mathbf{u} - \mathbf{u}_h) - \mathbf{J}^d(\alpha_z)\|_{\omega_z} = \inf_{\boldsymbol{\rho} \in \mathbf{RM}} \|\nabla(\mathbf{u} - \mathbf{u}_h - \boldsymbol{\rho})\|_{\omega_z} \leq C_{K,z}^{\text{loc}} \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|_{\omega_z}$$

With $C_K^{\text{loc}} := (d+1) \max\{C_{K,z}^{\text{loc}} : z \in \mathcal{V}_h\}$:

$$\begin{aligned} |(\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta, \nabla(\mathbf{u} - \mathbf{u}_h))| &\leq \frac{C_K^{\text{loc}}}{d+1} \sum_{z \in \mathcal{V}_h} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\|_{\omega_z} \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|_{\omega_z} \\ &\leq C_K^{\text{loc}} \left(\frac{1}{d+1} \sum_{z \in \mathcal{V}_h} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\|_{\omega_z}^2 \right)^{1/2} \left(\frac{1}{d+1} \sum_{z \in \mathcal{V}_h} \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|_{\omega_z}^2 \right)^{1/2} \\ &= C_K^{\text{loc}} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\| \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\| \end{aligned}$$

□

Weakly Symmetric Stress Equilibration: Upper Bound

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Weakly Symmetric Stress Equilibration: Upper Bound

$$\begin{aligned}(\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta, \nabla \mathbf{u} - \nabla \mathbf{u}_h) &\leq C_K^{\text{loc}} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\| \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\| \\ &\leq \frac{(C_K^{\text{loc}})^2}{2\delta} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\|^2 + \frac{\delta}{2} \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|^2\end{aligned}$$

\Rightarrow

$$\begin{aligned}\|\boldsymbol{\sigma}_h^\Delta\|_{C^{-1}}^2 &\geq \|\boldsymbol{\sigma}_h^R - \boldsymbol{\sigma}\|_{C^{-1}}^2 + \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|_C^2 \\ &\quad - \frac{(C_K^{\text{loc}})^2}{\delta} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\|^2 - \delta \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|^2 \\ &\geq \left(1 - \frac{\delta}{2\mu}\right) \|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|_C^2 - \frac{(C_K^{\text{loc}})^2}{\delta} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\|^2\end{aligned}$$

$\Rightarrow \quad (\delta = \mu)$

$$\|\boldsymbol{\varepsilon}(\mathbf{u} - \mathbf{u}_h)\|_C^2 \leq 2\|\boldsymbol{\sigma}_h^\Delta\|_{C^{-1}}^2 + \frac{2(C_K^{\text{loc}})^2}{\mu} \|\mathbf{as} \, \boldsymbol{\sigma}_h^\Delta\|^2$$

Weakly Symmetric Stress Equilibration: Lower Bound

Stress Equilibration: Basic Idea

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Weakly Symmetric Stress Equilibration: Lower Bound

h_z : local mesh size on ω_z

$$\|\sigma_{h,z}^\Delta\|_{\omega_z} \longrightarrow \min! \text{ s. t.}$$

$$\begin{aligned}(\operatorname{div} \sigma_{h,z}^\Delta, \mathbf{z})_T &= -((\mathbf{f} + \operatorname{div} \sigma(\mathbf{u}_h))\phi_z, \mathbf{z})_T \quad \forall \mathbf{z} \in P_k(T)^d, \quad T \subset \omega_z \\ \langle \llbracket \sigma_{h,z}^\Delta \cdot \mathbf{n} \rrbracket_S, \zeta \rangle_S &= -\langle \llbracket \sigma(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \zeta \rangle_S \quad \forall \zeta \in P_k(S)^d, \quad S \subset \omega_z \\ (\sigma_{h,z}^\Delta, \mathbf{J}^d(\gamma))_{\omega_z} &= 0 \quad \forall \gamma \in P_1(\mathcal{T}_h)|_{\omega_z} \cap H^1(\omega_z)\end{aligned}$$

Then, $\|\sigma_{h,z}^\Delta\|_{\omega_z}$ is bounded by the residual error estimator:

$$\|\sigma_{h,z}^\Delta\|_{\omega_z} \lesssim h_z \|\mathbf{f} + \operatorname{div} \sigma(\mathbf{u}_h)\|_{\omega_z} + \sum_{S \subset \omega_z} h_z^{1/2} \|\llbracket \sigma(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S\|_S$$

Idea of Proof:

$\|\sigma_{h,z}^\Delta\|_{\omega_z}$ bounded by suitably scaled linear combination of

$$|(\operatorname{div} \sigma_{h,z}^\Delta, \mathbf{z})_T|, \quad T \in \mathcal{T}_h \text{ and } \|\llbracket \sigma_h^\Delta \cdot \mathbf{n} \rrbracket_S\|_S, \quad S \in \mathcal{S}_h$$

(finite dimensional problem)

$$\text{Efficiency of residual estimator} \implies \|\sigma_{h,z}^\Delta\|_{\omega_z} \lesssim \|\varepsilon(\mathbf{u} - \mathbf{u}_h)\|_{\mathcal{C}, \omega_z}$$

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Hyperelasticity

Deformation gradient

$$\mathbf{F}(\mathbf{u}) = \mathbf{I} + \nabla \mathbf{u}$$

1st Piola-Kirchhoff stress tensor

$$\mathbf{P} = \partial_{\mathbf{F}} \psi(\mathbf{F}(\mathbf{u}))$$

For example: Neo-Hooke material (with $J(\mathbf{u}) = \det \mathbf{F}(\mathbf{u})$):

$$\mathbf{P} = \mu (\mathbf{F}(\mathbf{u}) - \mathbf{F}(\mathbf{u})^{-T}) + \frac{\lambda}{2} (J(\mathbf{u})^2 - 1) \mathbf{F}(\mathbf{u})^{-T}$$

Symmetry of Cauchy stress $\mathbf{P}\mathbf{F}(\mathbf{u})^T / J(\mathbf{u})$ (w.r.t. deformed configuration):

$$\mathbf{P}\mathbf{F}(\mathbf{u})^T = \mu (\mathbf{F}(\mathbf{u})\mathbf{F}(\mathbf{u})^T - \mathbf{I}) + \frac{\lambda}{2} (J(\mathbf{u})^2 - 1) \mathbf{I}$$

$$\mathbf{P}_h^R = \mathbf{P}(\mathbf{u}_h) + \mathbf{P}_h^\Delta \text{ with } \mathbf{P}_{h,z}^\Delta \in \boldsymbol{\Sigma}_{h,z}^\Delta \text{ s.t.}$$

$$(\operatorname{div} \mathbf{P}_{h,z}^\Delta, \mathbf{z})_T = -((\mathbf{f} + \operatorname{div} \mathbf{P}(\mathbf{u}_h))\phi_z, \mathbf{z})_T \quad \forall \mathbf{z} \in P_k(T)^d, \quad T \subset \omega_z$$

$$\langle \llbracket \mathbf{P}_{h,z}^\Delta \cdot \mathbf{n} \rrbracket_S, \boldsymbol{\zeta} \rangle_S = -\langle \llbracket \mathbf{P}(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \boldsymbol{\zeta} \rangle_S \quad \forall \boldsymbol{\zeta} \in P_k(S)^d, \quad S \subset \omega_z$$

$$(\mathbf{P}_{h,z}^\Delta \mathbf{F}(\mathbf{u}_h)^T, \mathbf{J}^d(\boldsymbol{\gamma}))_{\omega_z} = 0 \quad \forall \boldsymbol{\gamma} \in P_1(\mathcal{T}_h)|_{\omega_z} \cap H^1(\omega_z)$$

Extensions to Nonlinear Deformation Models

Hyperelasticity

Since $\mathbf{P}(\mathbf{u}_h) \notin \boldsymbol{\Sigma}_h$, in general, compute a projection $\widehat{\mathbf{P}}(\mathbf{u}_h) \in \boldsymbol{\Sigma}_h$ first

$\mathbf{P}_{h,z}^\Delta \in \boldsymbol{\Sigma}_{h,z}^\Delta$ s.t.

$$(\operatorname{div} \mathbf{P}_{h,z}^\Delta, \mathbf{z})_T = -((\mathbf{f} + \operatorname{div} \widehat{\mathbf{P}}(\mathbf{u}_h))\phi_z, \mathbf{z})_T \quad \forall \mathbf{z}$$

$$\langle \llbracket \mathbf{P}_{h,z}^\Delta \cdot \mathbf{n} \rrbracket_S, \boldsymbol{\zeta} \rangle_S = -\langle \llbracket \widehat{\mathbf{P}}(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \boldsymbol{\zeta} \rangle_S \quad \forall \boldsymbol{\zeta}$$

$$(\mathbf{P}_{h,z}^\Delta \mathbf{F}(\mathbf{u}_h)^T, \mathbf{J}^d(\boldsymbol{\gamma}))_{\omega_z} = -(\widehat{\mathbf{P}}(\mathbf{u}_h) \mathbf{F}(\mathbf{u}_h)^T \phi_z, \mathbf{J}^d(\boldsymbol{\gamma}))_{\omega_z} \quad \forall \boldsymbol{\gamma}$$

Symmetric stress elements would not be appropriate here!

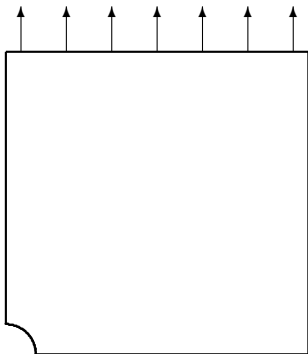
Kernel of the adjoint operator (linearly dependent constraints):

$$\mathbf{RM}(\mathbf{u}_h) = \operatorname{span}\left\{ \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}, \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}, \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, \begin{pmatrix} 0 \\ x_3 + (u_h)_3 \\ -(x_2 + (u_h)_2) \end{pmatrix}, \begin{pmatrix} -(x_3 + (u_h)_3) \\ 0 \\ x_1 + (u_h)_1 \end{pmatrix}, \begin{pmatrix} x_2 + (u_h)_2 \\ -(x_1 + (u_h)_1) \\ 0 \end{pmatrix} \right\}$$

[Bertrand/Moldenhauer/GS (2019), arXiv: 1903.05888]

Extensions to Nonlinear Deformation Models

(Perfect) Plasticity



Poisson ratio: $\nu = 0.29$

Boundary conditions:

$\boldsymbol{\sigma} \cdot \mathbf{n} = \mathbf{0}$ at right bdy and circle

$\boldsymbol{\sigma} \cdot \mathbf{n} = (0, \gamma)$ at upper bdy

Symmetry conditions:

$(\sigma_{11}, \sigma_{12}) \cdot \mathbf{n} = 0, u_2 = 0$ at bottom

$u_1 = 0, (\sigma_{21}, \sigma_{22}) \cdot \mathbf{n} = 0$ at left bdy

Load cycle: γ from 0 to 4.5 and then back

Load step size: $\delta\gamma = 0.025$

Plane strain

Collection of benchmark problems for elastoplasticity from
Stein/Wriggers/Rieger/Schmidt and Lang/Wieners/Wittum
in E. Stein (editor): Error-controlled Adaptive Finite Elements in Solid
Mechanics. Wiley, 2002

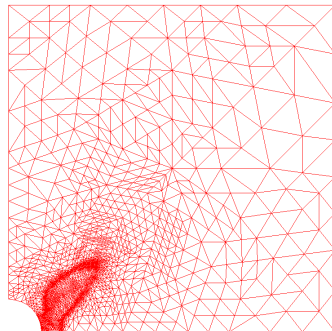
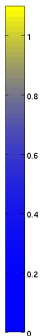
Extensions to Nonlinear Deformation Models

(Perfect) Plasticity

$\gamma = 4.0 :$

$|\mathbf{dev} \boldsymbol{\sigma}|$

triangulation



Extensions to Nonlinear Deformation Models

(Perfect) Plasticity

Admissible set for the stresses:

$$\mathcal{K}(t) = \{\boldsymbol{\sigma} \in H(\operatorname{div}, \Omega)^d : \operatorname{div} \boldsymbol{\sigma} + \mathbf{f} = \mathbf{0}, \text{ as } \boldsymbol{\sigma} = \mathbf{0} \text{ in } \Omega, \\ \boldsymbol{\sigma} \cdot \mathbf{n} = \ell(t) \text{ on } \Gamma_N, |\mathbf{dev} \boldsymbol{\sigma}| \leq \kappa \text{ in } \Omega\}$$

$\boldsymbol{\sigma}(\mathbf{u}_h) = \mathcal{P}_{\mathcal{K}(t)}(\mathcal{C}\boldsymbol{\varepsilon}(\mathbf{u}_h))$ not $H(\operatorname{div})$ -conforming, in general

$\boldsymbol{\sigma}_h^R = \boldsymbol{\sigma}(\mathbf{u}_h) + \boldsymbol{\sigma}_h^\Delta$ with $\boldsymbol{\sigma}_{h,z}^\Delta \in \boldsymbol{\Sigma}_{h,z}^\Delta$ s.t.

$$\begin{aligned} (\operatorname{div} \boldsymbol{\sigma}_{z,h}^\Delta, \mathbf{z})_{\omega_z} &= -((\mathbf{f} + \operatorname{div} \boldsymbol{\sigma}(\mathbf{u}_h))\phi_z, \mathbf{z})_{\omega_z} & \forall \mathbf{z} \\ \langle \llbracket \boldsymbol{\sigma}_{z,h}^\Delta \cdot \mathbf{n} \rrbracket_S, \boldsymbol{\zeta} \rangle_S &= -\langle \llbracket \boldsymbol{\sigma}(\mathbf{u}_h) \cdot \mathbf{n} \rrbracket_S \phi_z, \boldsymbol{\zeta} \rangle_S & \forall \boldsymbol{\zeta} \\ (\boldsymbol{\sigma}_{z,h}^\Delta, \mathbf{J}^d(\boldsymbol{\gamma}))_{\omega_z} &= 0 & \forall \boldsymbol{\gamma} \\ (\widehat{\mathbf{N}} : (\mathbf{dev} \boldsymbol{\sigma}_{h,z}^\Delta), \vartheta)_{\omega_z} &= -((\kappa + \mathbf{dev} \boldsymbol{\sigma}(\mathbf{u}_h))\phi_z, \vartheta)_{\omega_z} & \forall \vartheta \in X^a \end{aligned}$$

with $\widehat{\mathbf{N}} = \frac{\mathbf{dev} \widehat{\boldsymbol{\sigma}}}{|\mathbf{dev} \widehat{\boldsymbol{\sigma}}|}$, X^a : set of active constraints

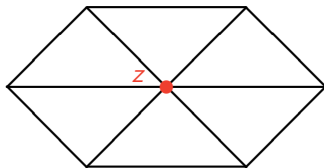
Extensions to Nonlinear Deformation Models

(Perfect) Plasticity

$$\hat{\mathbf{N}} \in \mathbb{R}^{2 \times 2} \text{ with } |\hat{\mathbf{N}}| = 1$$

$$\hat{\mathbf{N}} = \alpha_d \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix} + \alpha_e \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} + \alpha_a \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

$$\text{with } 2(\alpha_d^2 + \alpha_e^2 + \alpha_a^2) = 1, \alpha_d \neq 0$$



$$\inf_{\mathbf{z}, \gamma, \vartheta} \sup_{\boldsymbol{\tau} \in \boldsymbol{\Sigma}_{\mathbf{z}, h}^{\Delta}} \frac{(\operatorname{div} \boldsymbol{\tau}, \mathbf{z})_{\omega_z} + (\boldsymbol{\tau}, \mathbf{J}^2(\gamma))_{\omega_z} + (\hat{\mathbf{N}} : \operatorname{dev} \boldsymbol{\tau}, \vartheta)_{\omega_z}}{\|\boldsymbol{\tau}\|_{H(\operatorname{div}, \omega_z)} (\|\mathbf{z}\|_{\omega_z} + \|\gamma\|_{\omega_z} + \|\vartheta\|_{\omega_z})} \geq \beta > 0$$

Extensions to Nonlinear Deformation Models

(Perfect) Plasticity

Dimension of subspace with

$$\sup_{\boldsymbol{\tau} \in \boldsymbol{\Sigma}_{z,h}^{\Delta}} \frac{(\operatorname{div} \boldsymbol{\tau}, \mathbf{z})_{\omega_z} + (\boldsymbol{\tau}, \mathbf{J}^2(\boldsymbol{\gamma}))_{\omega_z} + (\widehat{\mathbf{N}} : \mathbf{dev} \boldsymbol{\tau}, \vartheta)_{\omega_z}}{\|\boldsymbol{\tau}\|_{H(\operatorname{div}, \omega_z)} (\|\mathbf{z}\|_{\omega_z} + \|\boldsymbol{\gamma}\|_{\omega_z} + \|\vartheta\|_{\omega_z})} = 0 :$$

$\boldsymbol{\Sigma}_z \setminus \mathbf{Z}/\mathbf{R}/X:$	$DP_1/DP_1/DP_1$	$DP_1/P_1/DP_1$	$DP_1/P_1/P_1$	$P_1/P_1/P_1$
RT_1^2	24	13	8	4
$RT_1^2 + \nabla^{\perp} B_3^{\text{cf}}$	12	8	6	4
$RT_1^2 + \nabla^{\perp} B_3^{\text{nc}}$	4	4	4	4

$$B_3^{\text{cf}} = \{\mathbf{b} \in P_3(\mathcal{T})^2 : \mathbf{b}|_E = 0 \text{ for all edges } E\}$$

$$B_3^{\text{nc}} = \{\mathbf{b} \in P_3(\mathcal{T})^2 : \langle \mathbf{b}, \mathbf{q} \rangle_E = 0 \text{ for all } \mathbf{q} \in P_1(E)^2 \text{ and all edges } E\}$$

Related to symmetric stress method by

Gopalakrishnan/Guzmán (SIAM J. Numer. Anal., 2011)

See also: Kober/GS (2018, ENUMATH-Proceedings)

Extensions to Nonlinear Deformation Models

(Perfect) Plasticity

Null space of the adjoint operator (linearly dependent constraints):

$$\mathbf{z} = \begin{pmatrix} 1 \\ 0 \end{pmatrix}, \gamma = \mathbf{0}, \vartheta = 0$$

$$\mathbf{z} = \begin{pmatrix} 0 \\ 1 \end{pmatrix}, \gamma = \mathbf{0}, \vartheta = 0$$

$$\mathbf{z} = \begin{pmatrix} x_2 \\ -x_1 \end{pmatrix}, \gamma = 2 \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix}, \vartheta = 0 \quad (\text{rigid body modes})$$

and an additional plastic mode

$$\mathbf{z} = \alpha_d \begin{pmatrix} x_1 \\ -x_2 \end{pmatrix} + \alpha_e \begin{pmatrix} x_2 \\ x_1 \end{pmatrix}, \gamma = \mathbf{0}, \vartheta = 2$$

Conclusions and References

Conclusions and References

Weakly symmetric stress equilibration

Computable (and reasonably close) upper bounds for linear elasticity

Extension to nonlinear material models (hyperelasticity, plasticity)
requires modifications!

Bertrand/Kober/Moldenhauer/GS:

Weakly Symmetric Stress Equilibration and A Posteriori Error Estimation
for Linear Elasticity.

arXiv: 1808.02655

Bertrand/Moldenhauer/GS:

Weakly Symmetric Stress Equilibration for Hyperelastic Material Models.

arXiv: 1903.05888